

Numerical Simulations of MHD turbulence at low to moderate magnetic Reynolds number

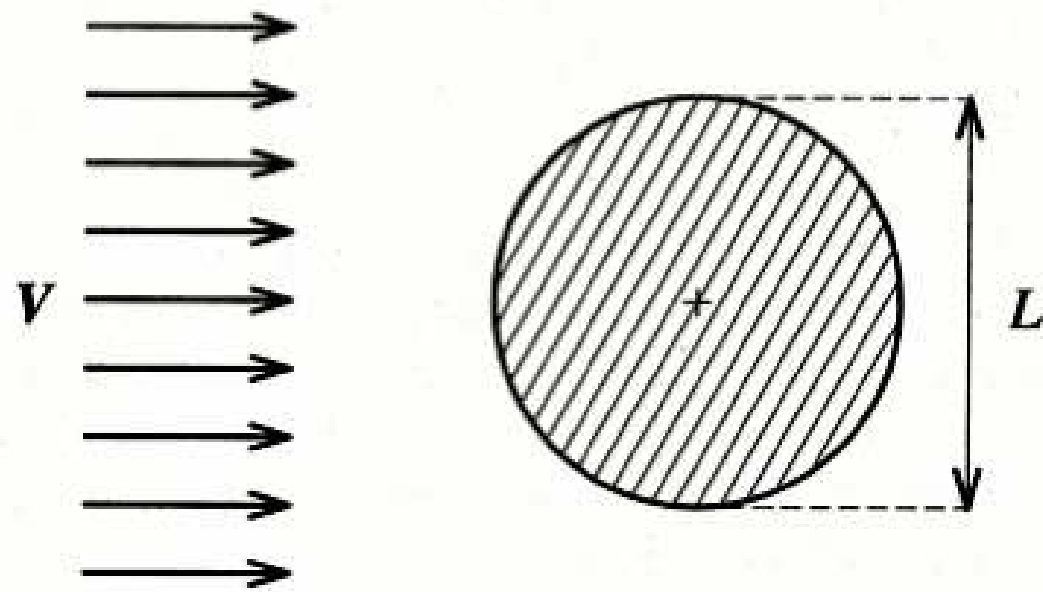
Bernard Knaepen*
(Thessaloniki, October 2003)

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Plan

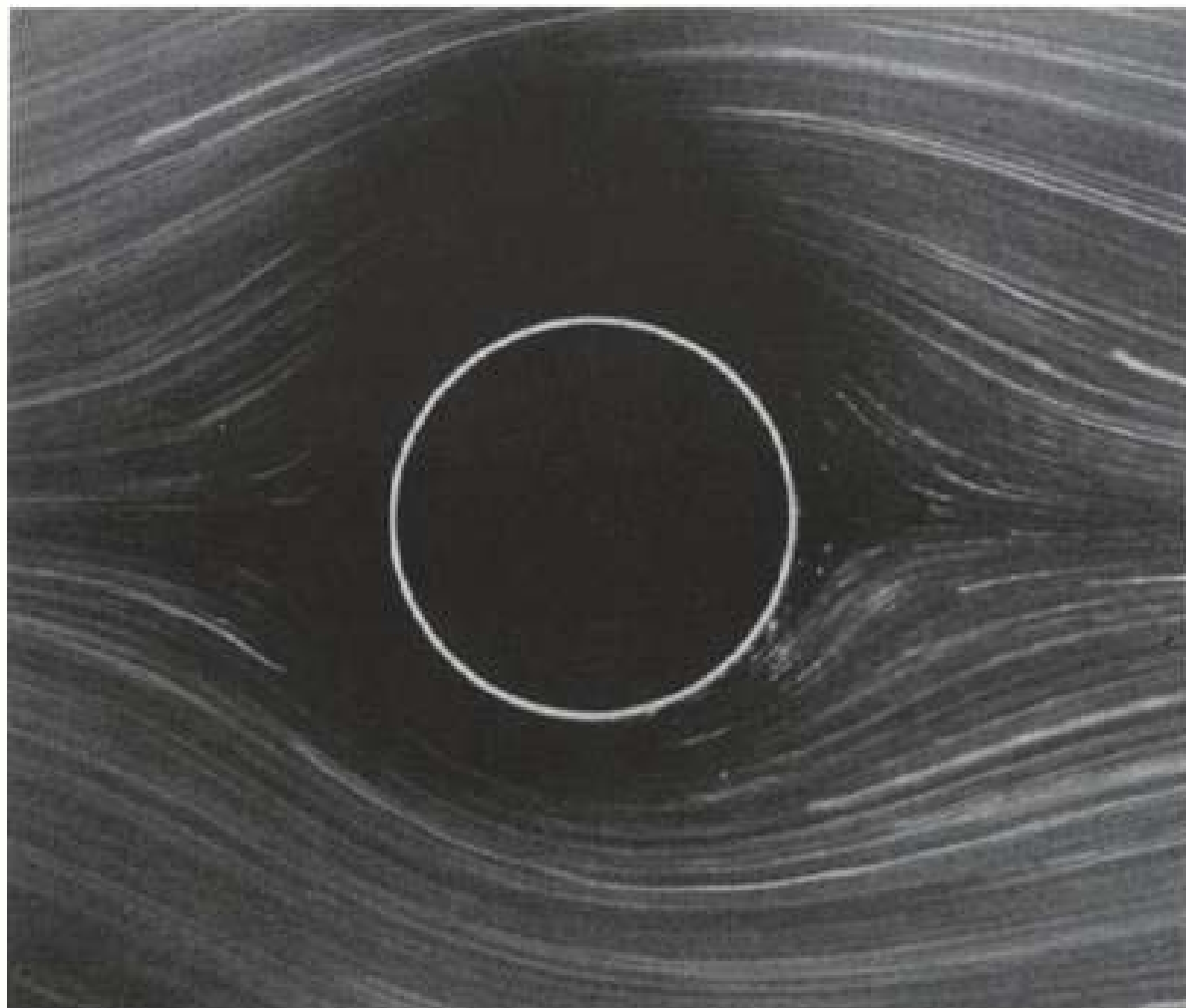
- Description of turbulence (hydrodynamics)
 - Examples
 - Phenomenology
 - Overview of Large-Eddy Simulations (LES)
- MHD
 - LES in the quasi-static approximation
- Prospects

“Definition” of Turbulence (I)



Reynolds number:

$$Re = \frac{VL}{\mu} \quad (\text{non-dimensional number})$$



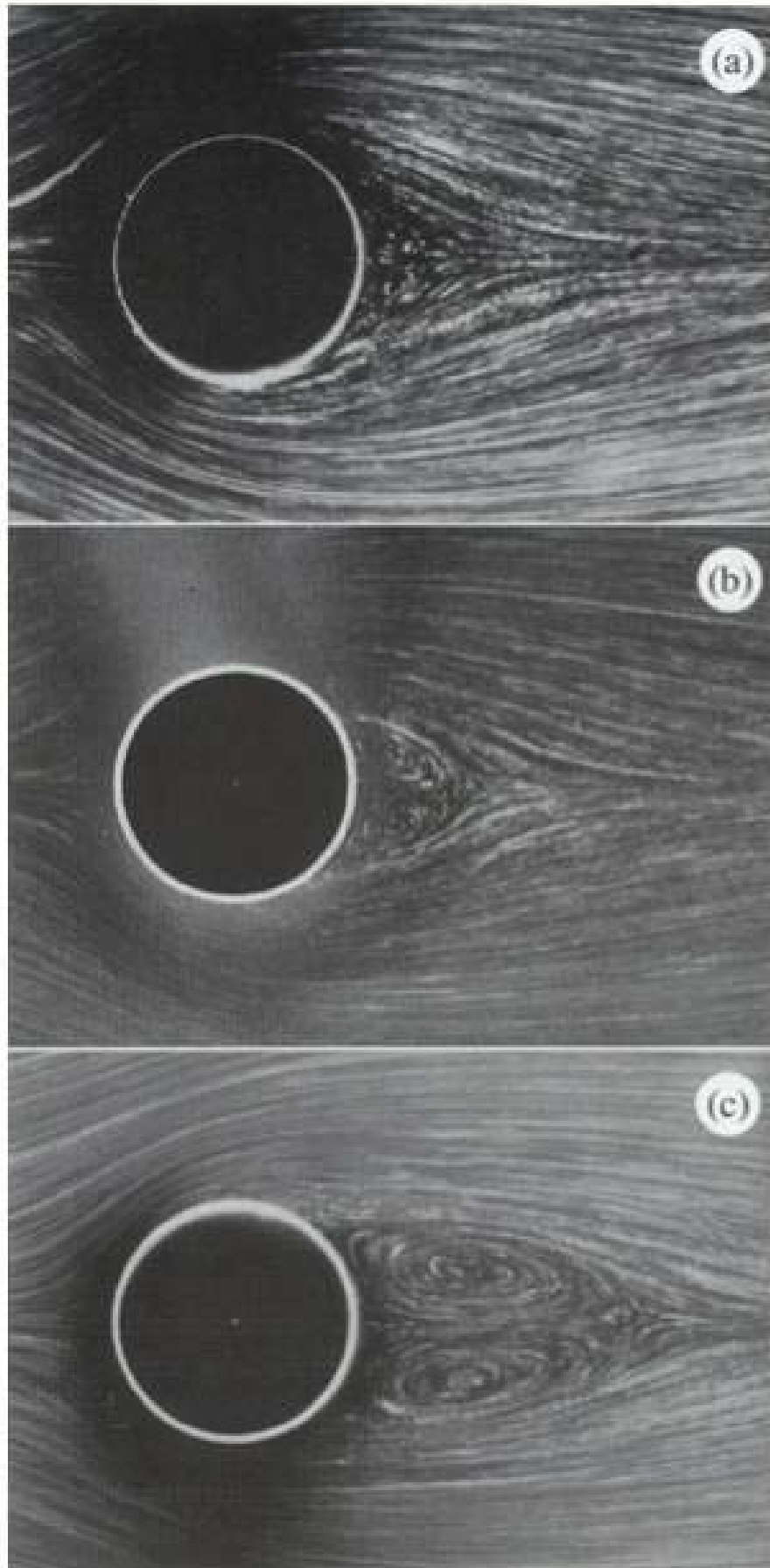
If Re is small

→ laminar flow

$$Re = 1.54$$

(Photo: Van Dyke M. An Album of Fluid Motion)

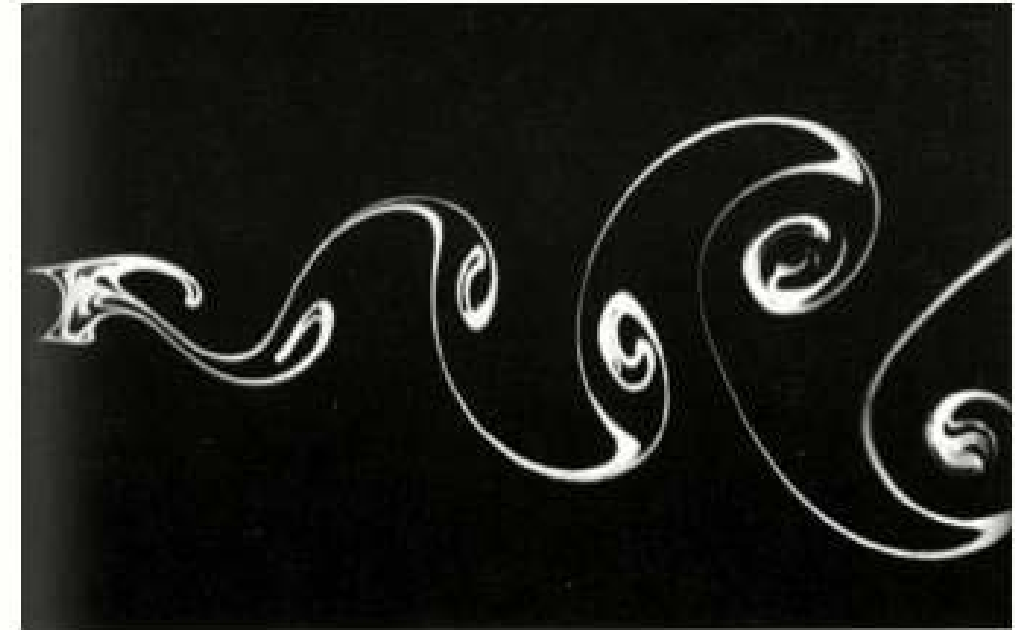
“Definition” of Turbulence (II)



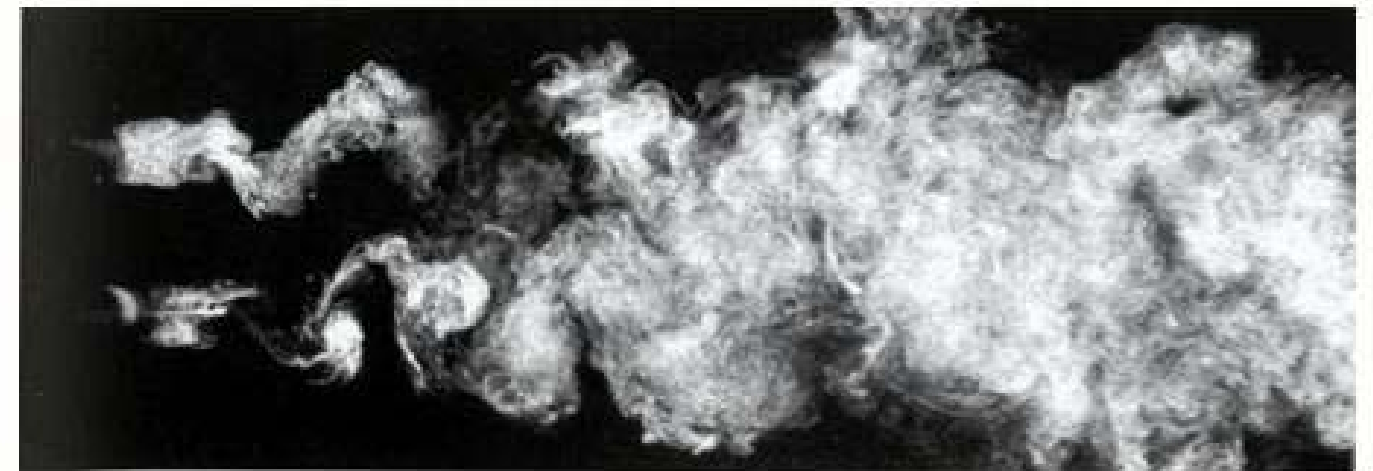
$Re = 9.6$

$Re = 13.1$

$Re = 26$



$Re = 140$



$Re = 1800$

(Photo: Van Dyke M. An Album of Fluid Motion)

Turbulence: examples (II)



<http://www.nasa.gov>

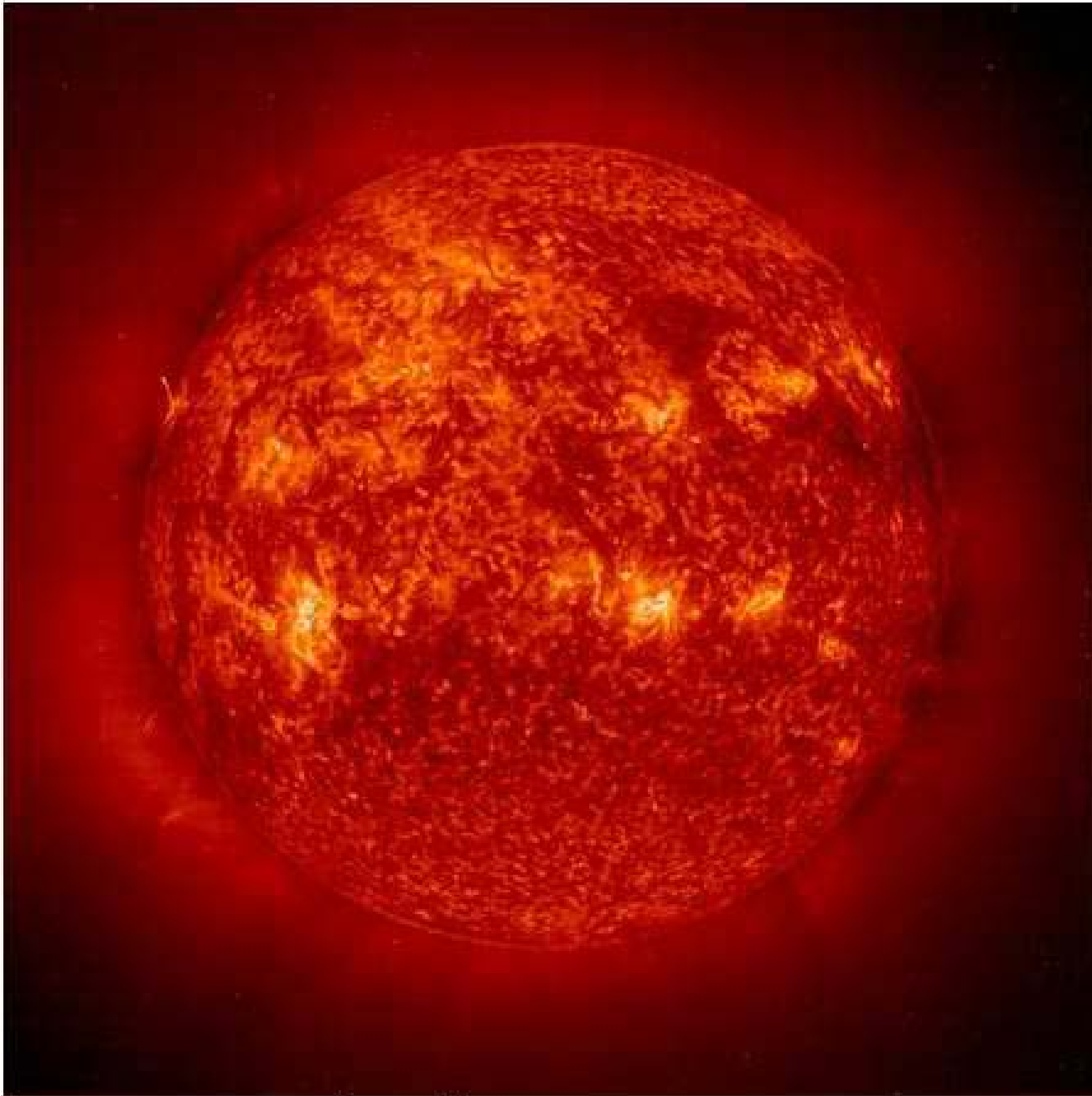
Cyclone (Earth)



<http://www.nasa.gov>

Red spot (Jupiter)

Turbulence: examples (III)



<http://www.nasa.gov>

Convection (Sun)



<http://www.nasa.gov>

Star formation
(gaz cloud)

Navier–Stokes equations

Incompressible flow (non MHD):

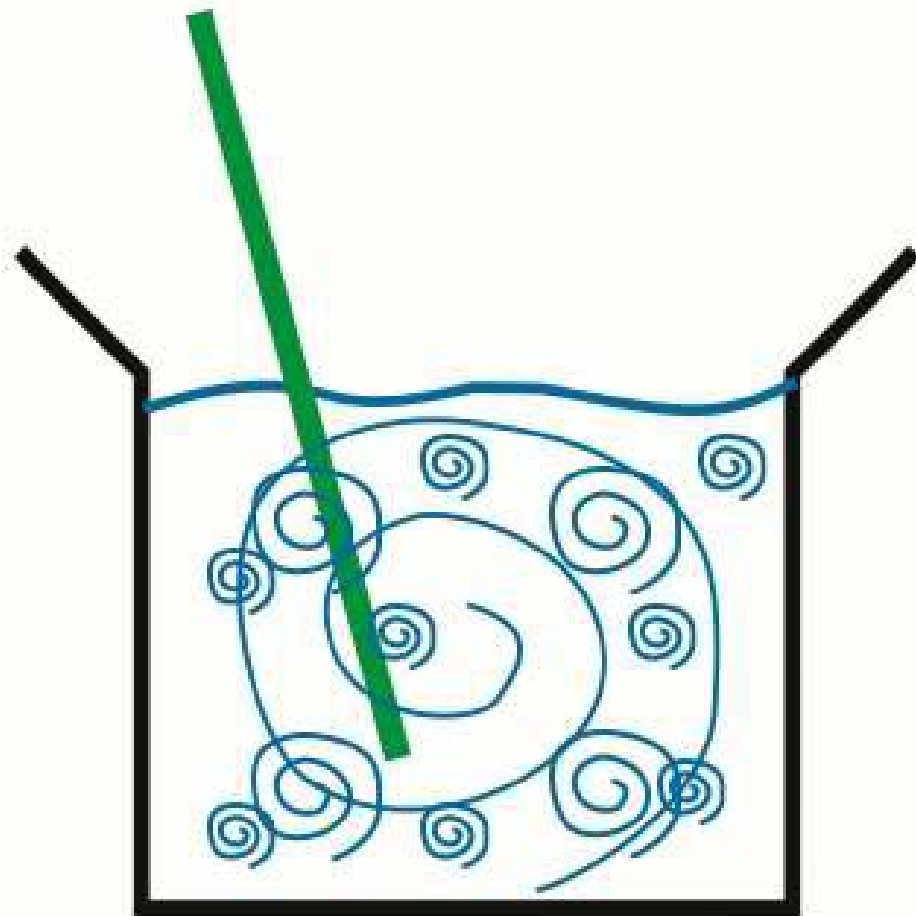
$$\partial_t u_i + u_j \partial_j u_i = -\partial_i(p/\rho) + \nu \Delta u_i, \quad \partial_i u_i = 0$$

+ initial condition: $u_i(\mathbf{x}, t = 0) = u_i^0(\mathbf{x})$

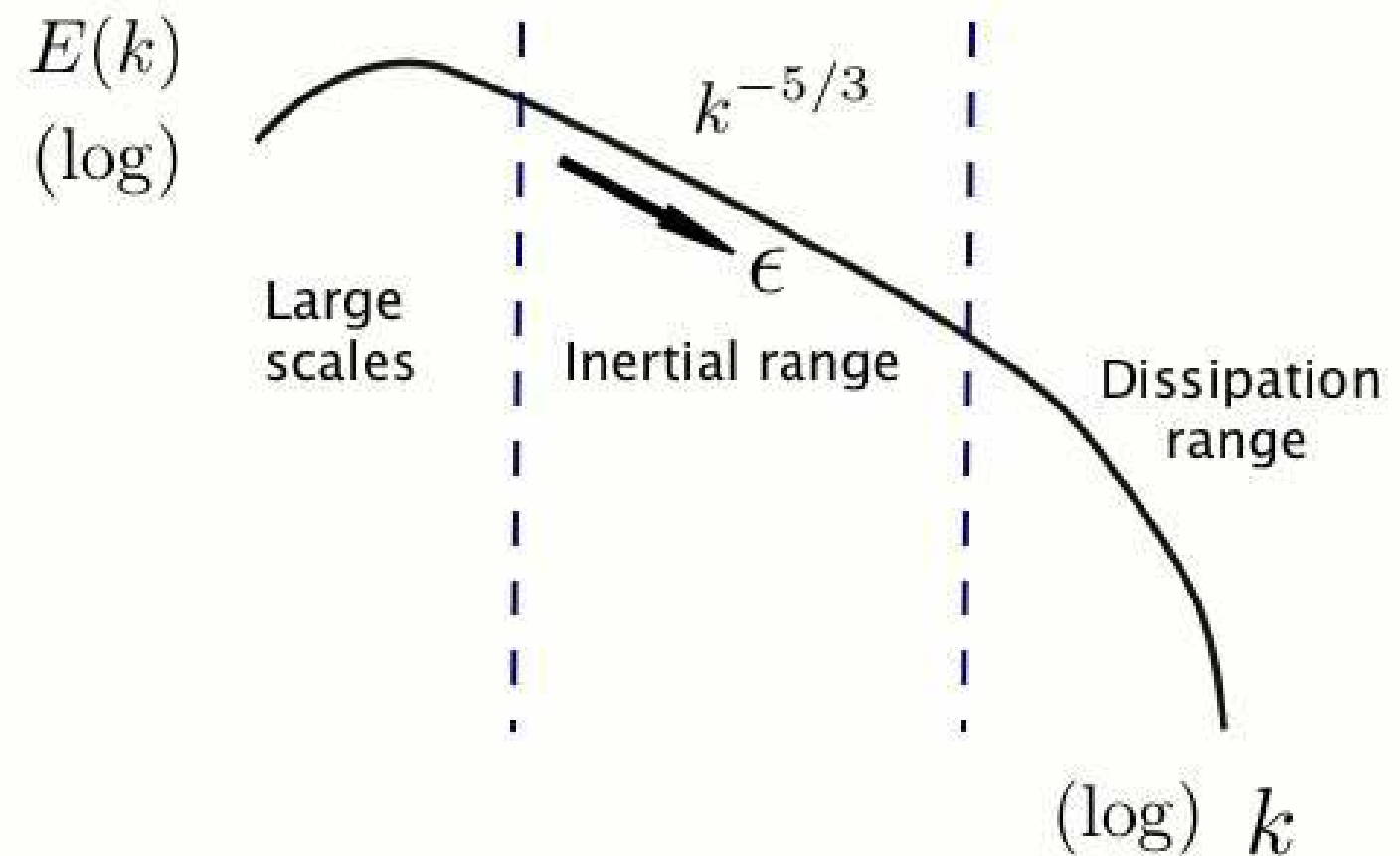
+ boundary conditions

➡ Millenium Prize: <http://www.claymath.org>

Kolmogorov phenomenology (1941)

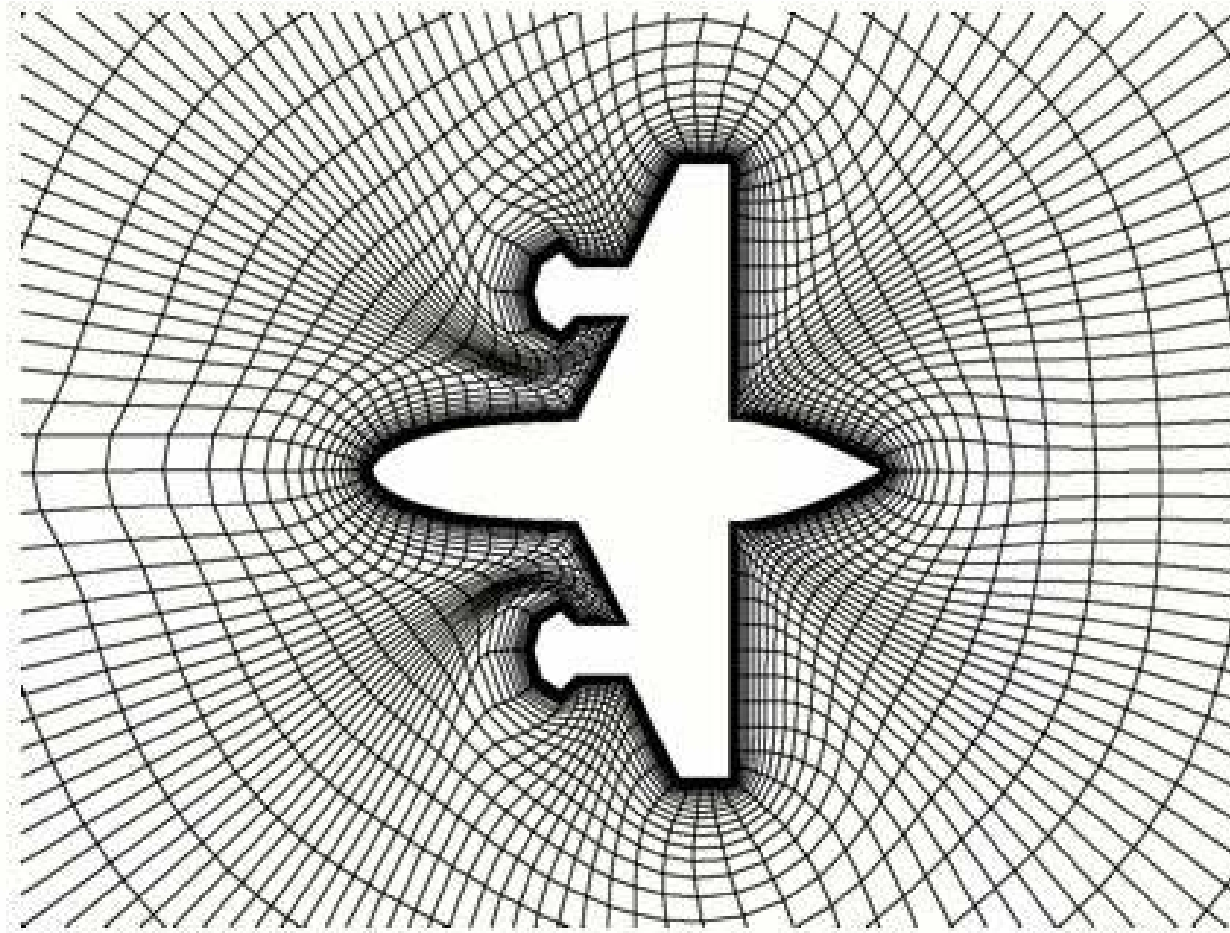


$$\mathbf{u}(\mathbf{k}) = \int \mathbf{u}(\mathbf{x}) e^{-i\mathbf{k} \cdot \mathbf{x}} d\mathbf{x}$$



$$E(k) = K \epsilon^{2/3} k^{-5/3}$$

Direct numerical simulations (DNS)



- Step 1: grid generation
- Step 2: Navier–Stokes equations discretization

$$\partial_t u_i + u_j \partial_j u_i = -\partial_i(p/\rho) + \nu \Delta u_i$$

$$\Rightarrow \partial_t u_i = F(x_k) + O(\delta^n)$$

$(\delta/L \ll 1)$

Direct numerical simulations (DNS)

Is turbulence a solved problem? $\Rightarrow$ NO

- Not satisfying from the theoretical point of view.
- Inapplicable for most flows encountered in nature or industrial applications.

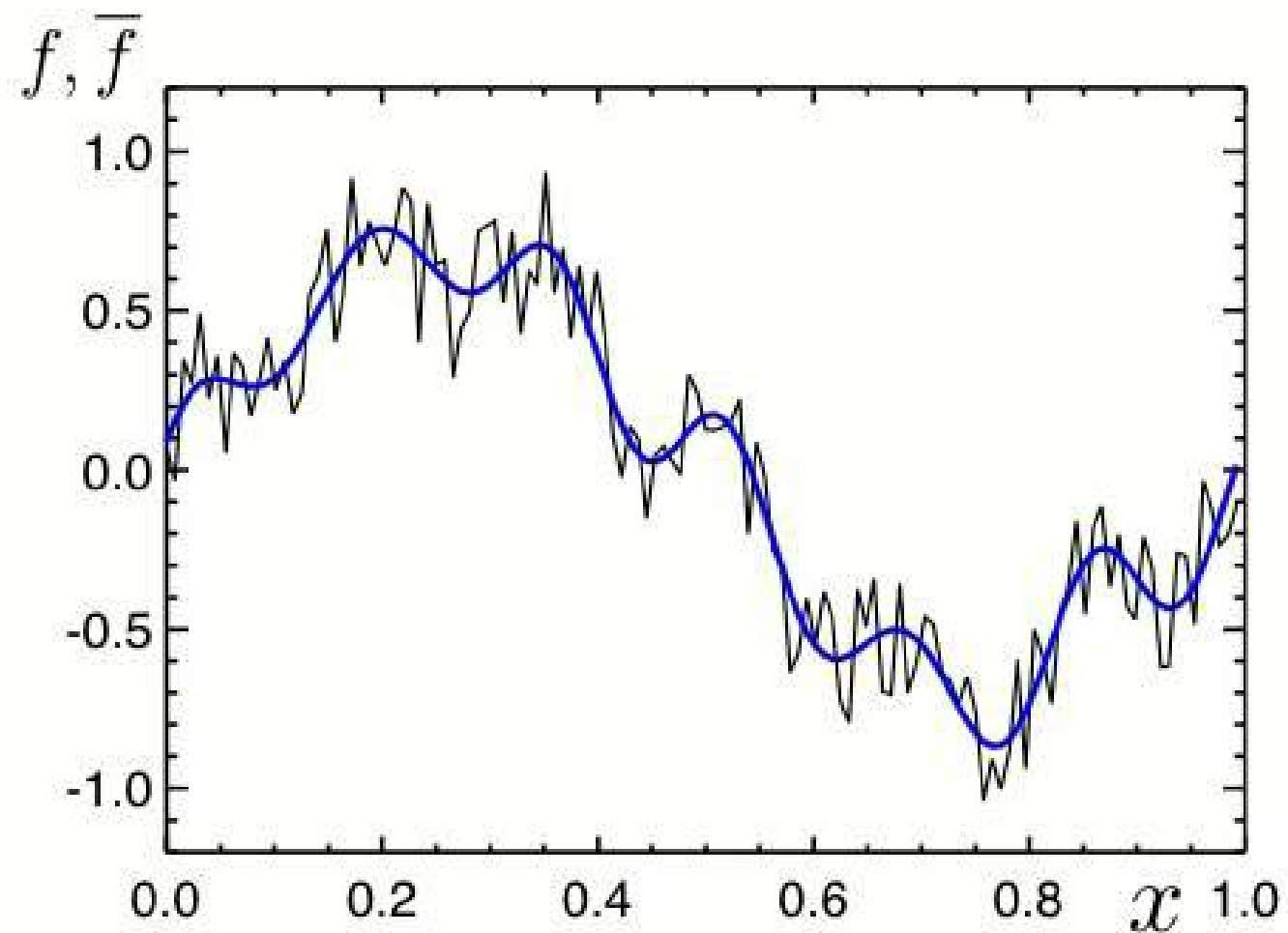
$$\# \text{ of grid points} \sim Re^{9/4}$$

- Commercial aircraft: $Re = 10^8 \Rightarrow 10^{18}$ grid points
“Teraflops” computer ($10^{12}/s$) $\Rightarrow$ 1s of flight $\approx$ 1000 years of computing time

But:

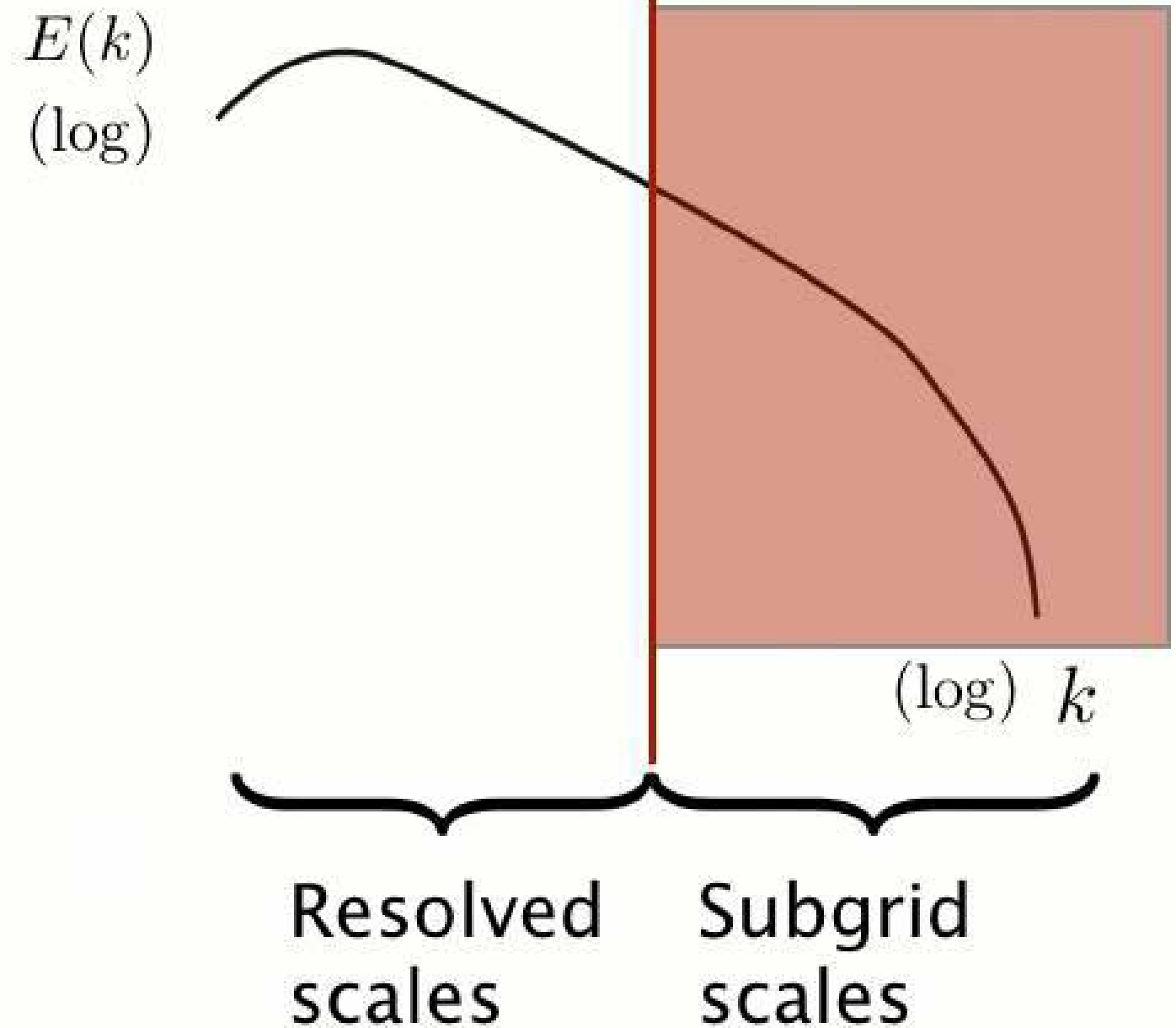
DNS provide accurate and non-intrusive measurements for flows at low Reynolds numbers and are efficient to validate and test models and approximate methods.

Large-Eddy Simulations (LES)



- Complete signal
- Resolved signal = LES signal

$$F : f(x) \rightarrow \bar{f}(x)$$



Large-Eddy Simulations (II)

Navier–Stokes equations:

$$\partial_t u_i + u_j \partial_j u_i = -\partial_i (p/\rho) + \nu \Delta u_i$$

$$\overline{u_j \partial_j u_i} \neq \bar{u}_j \partial_j \bar{u}_i \Rightarrow [F, P] \neq 0 \quad P : \text{product}$$

$$\partial_t \bar{u}_i + \bar{u}_j \partial_j \bar{u}_i = -\partial_i (\bar{p}/\rho) + \nu \Delta \bar{u}_i + (\bar{u}_j \partial_j \bar{u}_i - \overline{u_j \partial_j u_i})$$

Filtered Navier–Stokes equations (LES):

$$\partial_t \bar{u}_i + \bar{u}_j \partial_j \bar{u}_i = -\partial_i (\bar{p}/\rho) + \nu \Delta \bar{u}_i - \partial_j \tau_{ij}$$

$$\tau_{ij} = [F, P](u_i, u_j) : \text{subgrid-scale stress tensor}$$

$$\tau_{ij} = \overline{u_i u_j} - \bar{u}_i \bar{u}_j$$

Large-Eddy Simulations (III)

➔ τ_{ij} needs to be modelled to close the equations

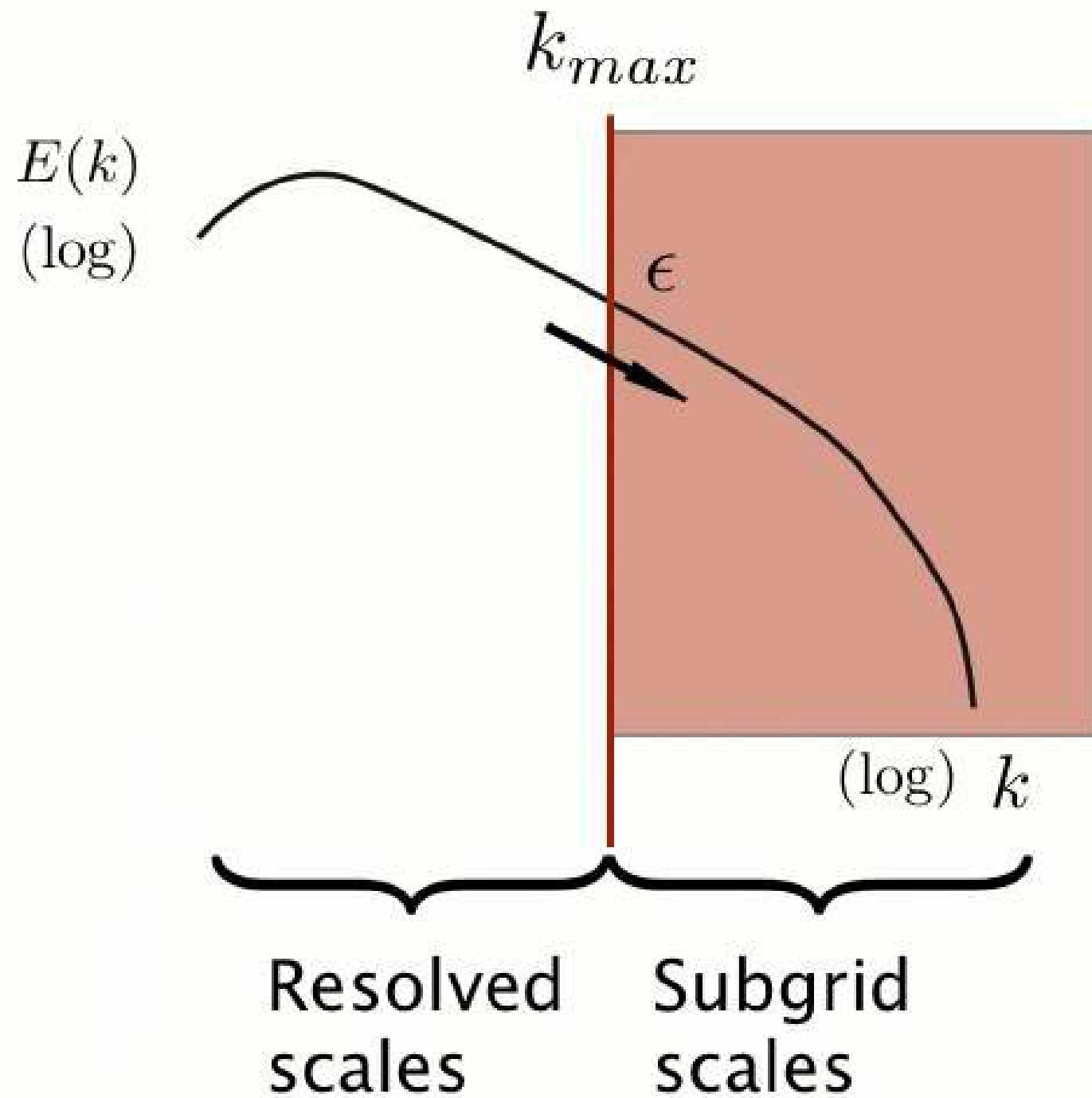
$$\tau_{ij}^M = \tau_{ij}^M(\bar{u}_i) \approx \tau_{ij}$$

● How to model τ_{ij} ? ➔ eddy viscosity

$$\tau_{ij} = -2\nu_t S_{ij} \quad \text{with} \quad S_{ij} = \frac{1}{2}(\partial_i \bar{u}_j + \partial_j \bar{u}_i)$$

$$\nu \rightarrow \nu + \nu_t \quad (\text{homogeneous turbulence})$$

Kolmogorov model



$$[\nu_t] = L^2 T^{-1}$$

$$[\epsilon] = L^2 T^{-3}$$

$$\overline{\Delta} \sim \frac{1}{k_{max}}$$

$$[\overline{\Delta}] = L$$

$$\nu_t = C_\nu \epsilon^{1/3} \Delta^{4/3}$$

(Kolmogorov model)

Smagorinski model

$$\partial_t \bar{u}_i + \bar{u}_j \partial_j \bar{u}_i = -\partial_i(\bar{p}/\rho) + \nu \Delta \bar{u}_i - \partial_j \tau_{ij}$$

$$\Rightarrow \epsilon_\tau = u_i \partial_j \tau_{ij} = -S_{ij} \tau_{ij}$$

$$= -S_{ij}(-2C_\nu \epsilon^{1/3} \Delta^{4/3} S_{ij}) = 2C_\nu \epsilon^{1/3} \Delta^{4/3} (S_{ij} S_{ij})$$

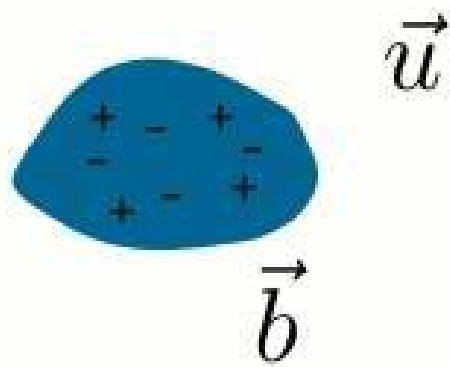
Hypothesis: $\epsilon_\tau = \epsilon$

$$\epsilon = \Delta^2 [C_\nu (2S_{ij} S_{ij})]^{3/2}$$

$$\tau_{ij} = -2C \Delta^2 \sqrt{2S_{ij} S_{ij}} S_{ij} \quad (C = C_\nu^{3/2})$$

C is the Smagorinski constant (only parameter)

Magnetohydrodynamics

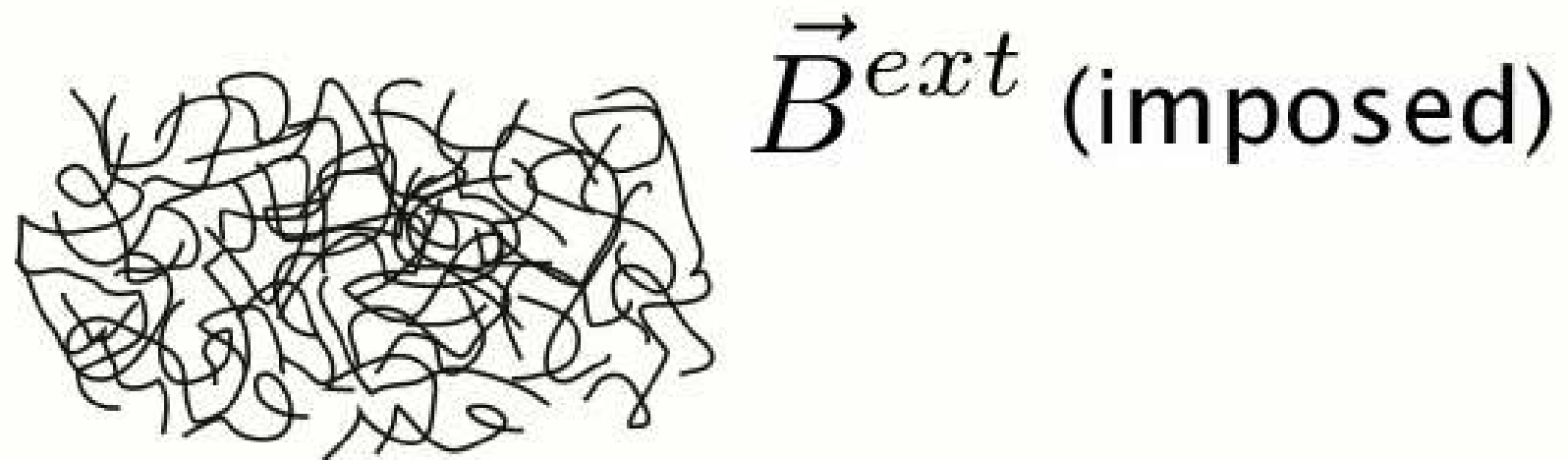


$$\partial_t u_i = -\partial_i(p/\rho) - u_j \partial_j u_i + b_j \partial_j b_i + \nu \Delta u_i$$

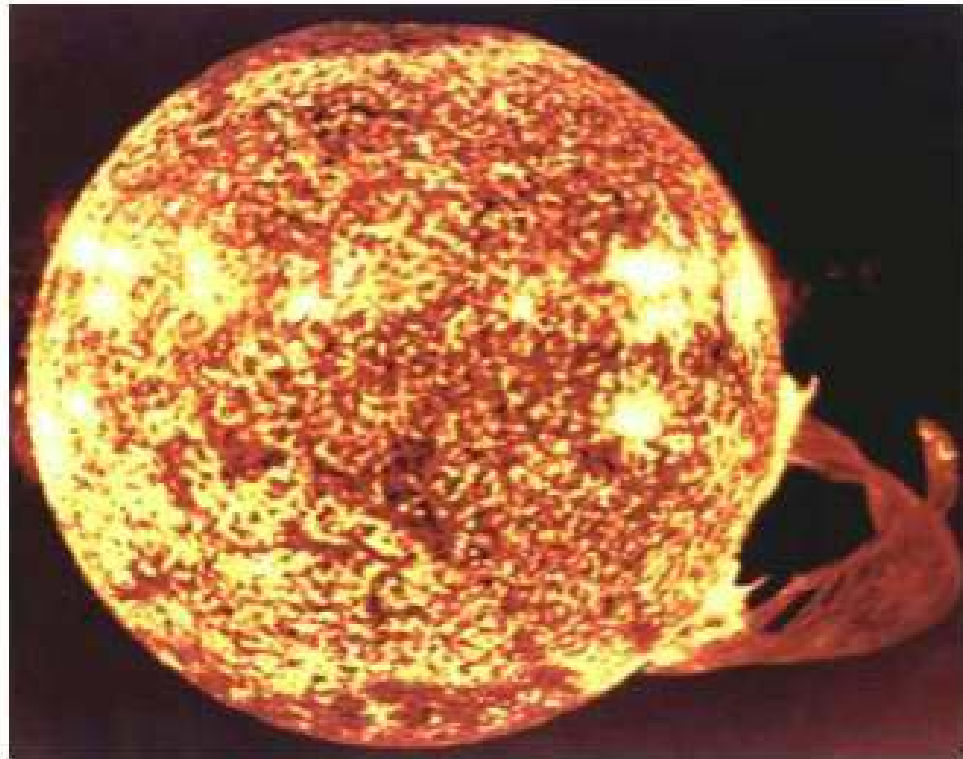
$$\partial_t b_i = -u_j \partial_j b_i + b_j \partial_j u_i + \eta \Delta b_i$$

$$\partial_i u_i = 0$$

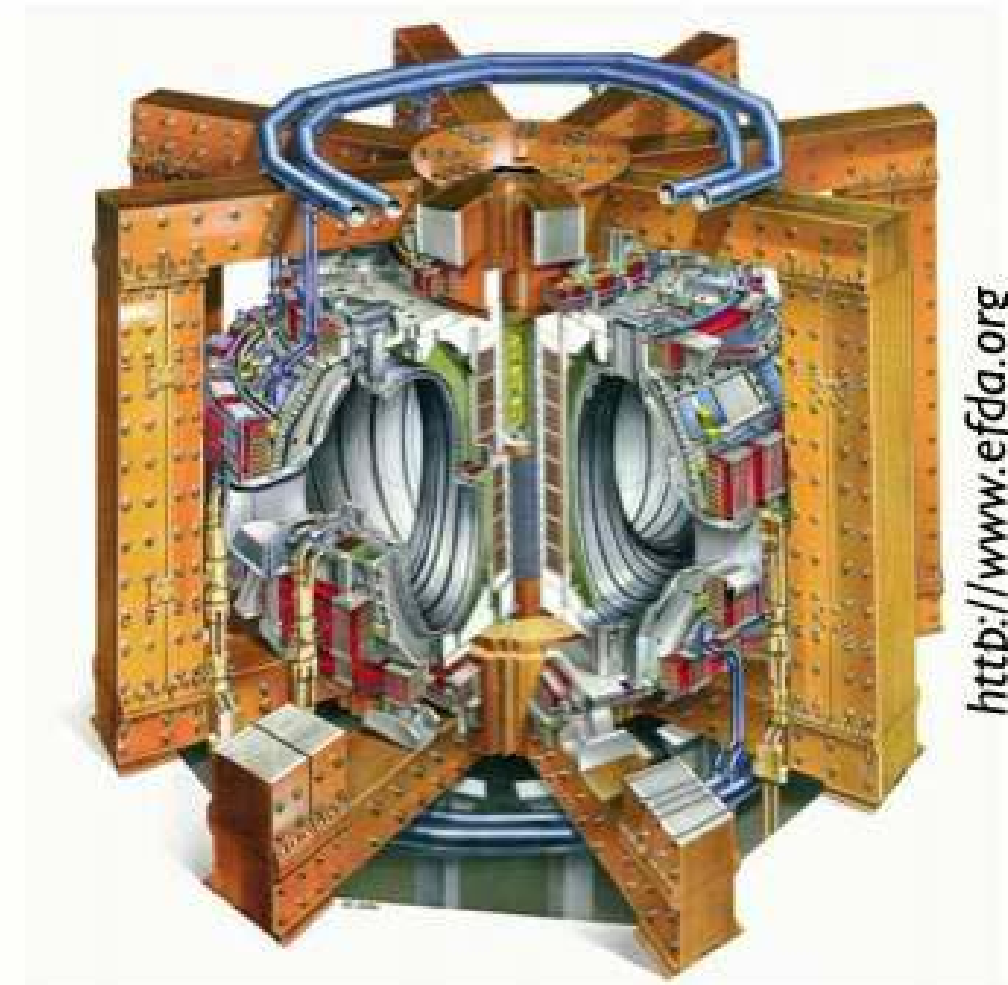
$$\partial_i b_i = 0$$



Motivations



(<http://www.nasa.gov>)



<http://www.efda.org>

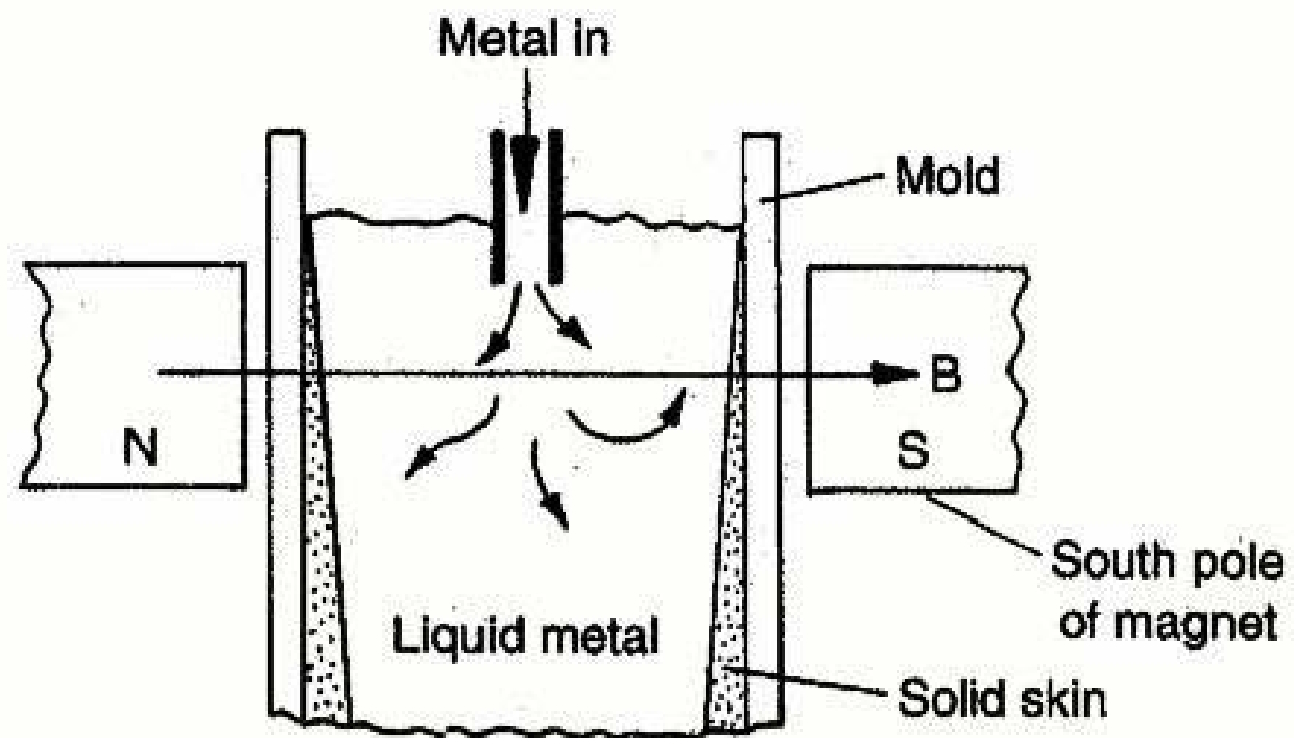
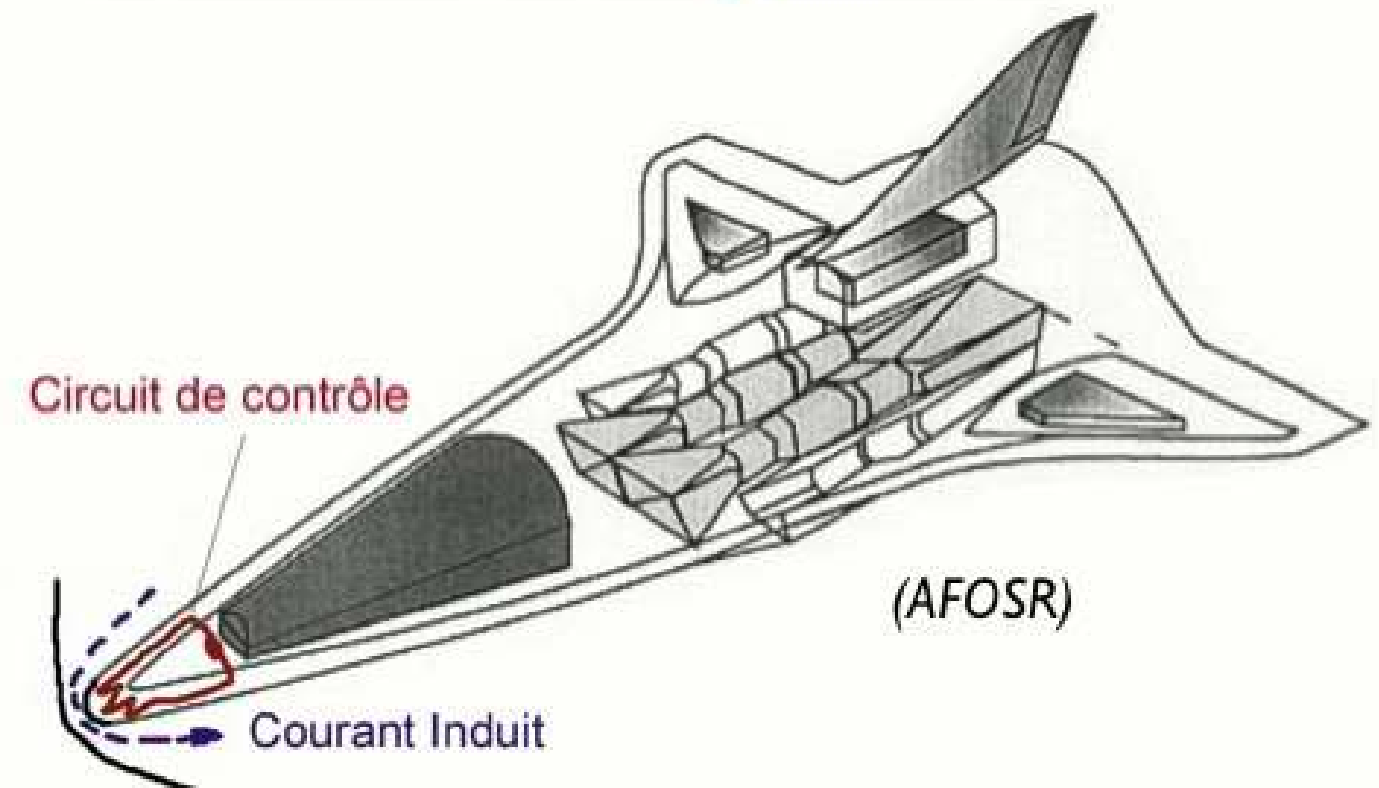
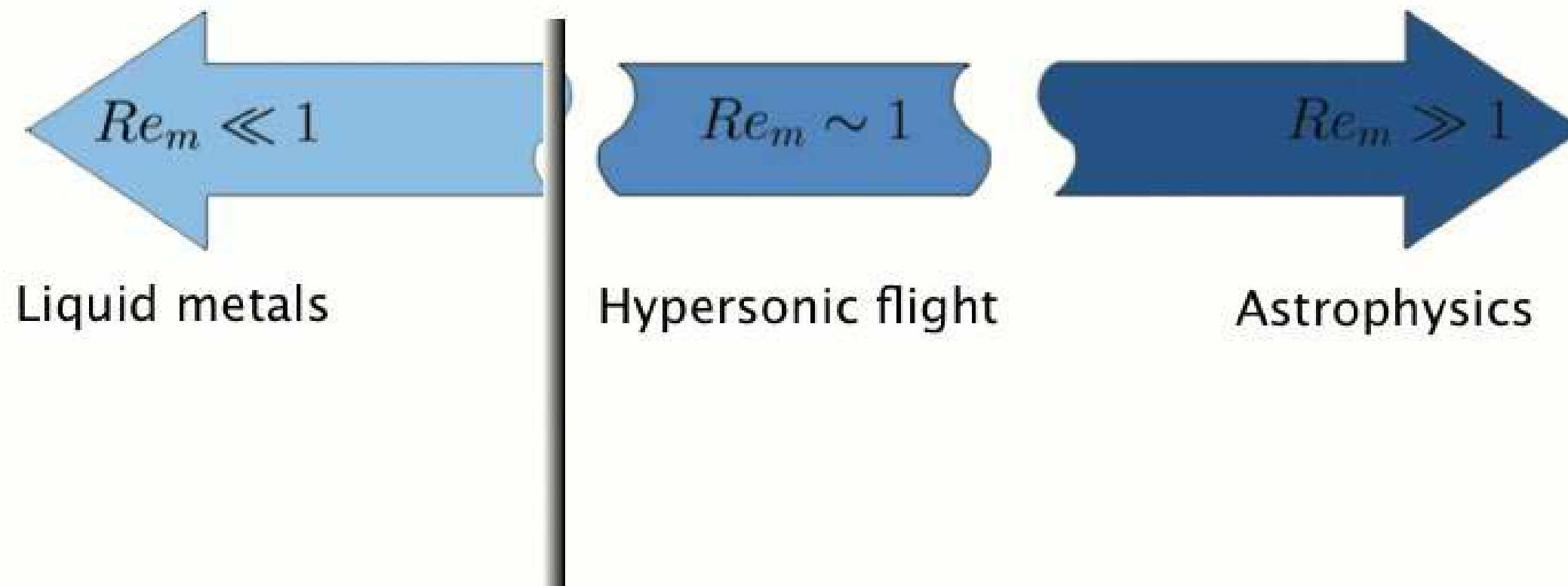


Figure I.5 Magnetic damping.
(Davidson, 2001)



Magnetic Reynolds number

$$\partial_t b_i = -u_j \partial_j b_i + b_j \partial_j u_i + \eta \Delta b_i \quad \Rightarrow \quad Re_m = \frac{uL}{\eta}$$



$Re_m \ll 1$: Quasi-Static approximation

Quasi-Static approximation

$$\partial_t b_i = -u_j \cancel{\partial_j b_i} + b_j \cancel{\partial_j u_i} + B_j^{ext} \partial_j u_i + \eta \Delta b_i$$

➔ 'steady state' $0 = B_j^{ext} \partial_j u_i + \eta \Delta b_i$

$$\partial_t u_i = -\partial_i(p/\rho) - u_j \partial_j u_i + \frac{1}{(\mu\rho)} b_j \cancel{\partial_j b_i} + \frac{1}{(\mu\rho)} B_j^{ext} \partial_j b_i + \nu \Delta u_i$$

$$\partial_t u_i = -\partial_i(p/\rho) - u_j \partial_j u_i + \frac{(B_z^{ext})^2}{\mu\eta\rho} \Delta^{-2} \partial_z \partial_z u_i + \nu \Delta u_i$$

Quasi-Static approximation

QS approximation: Large-Eddy Simulation

$$\partial_t u_i = -\partial_i(p/\rho) - u_j \partial_j u_i + \frac{(B_z^{ext})^2}{\mu\eta\rho} \Delta^{-2} \partial_z \partial_z u_i + \nu \Delta u_i$$

Intensity parameter:

$$N = \frac{(B_z^{ext})^2 L}{\mu\eta\rho\nu}$$

N=1: magnetic effects ~ non-linear effects

N=10: magnetic effects ~ 10 x non-linear effects

LES:

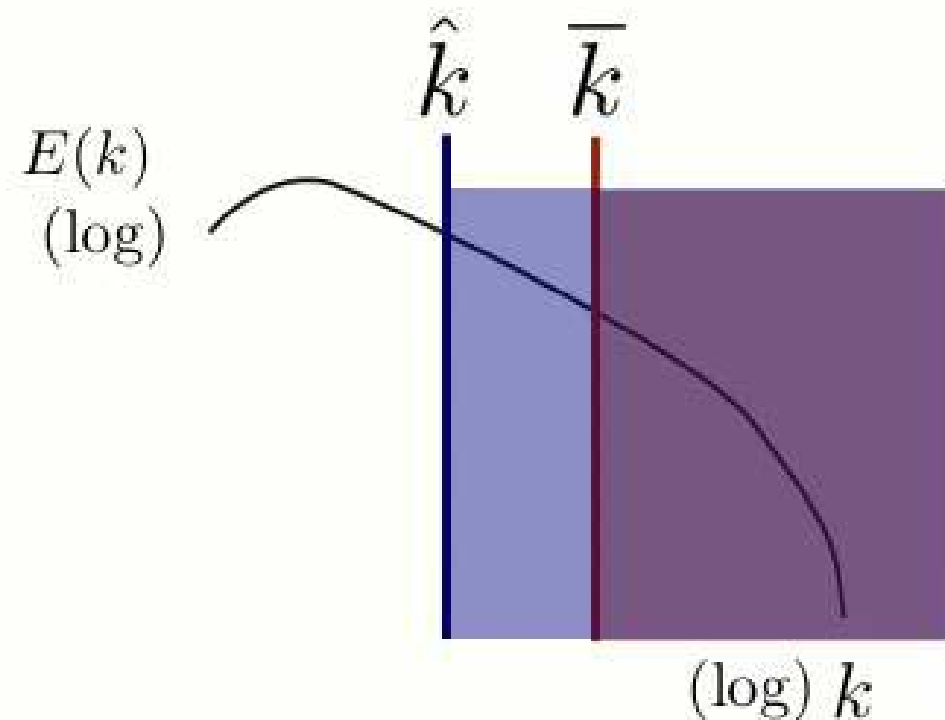
$$\partial_t \bar{u}_i = -\partial_i(\bar{p}/\rho) - \bar{u}_j \partial_j \bar{u}_i + \frac{(B_z^{ext})^2}{\mu\eta\rho} \Delta^{-2} \partial_z \partial_z \bar{u}_i + \nu \Delta \bar{u}_i - \partial_j \tau_{ij}$$

$$\tau_{ij} = \overline{u_i u_j} - \bar{u}_i \bar{u}_j$$

Dynamic procedure

$$\tau_{ij} = -2C\Delta^2 \sqrt{2S_{ij}S_{ij}}S_{ij} \quad (\text{Smagorinski})$$

One parameter: Smagorinski constant C



- Self-similarity in the inertial range

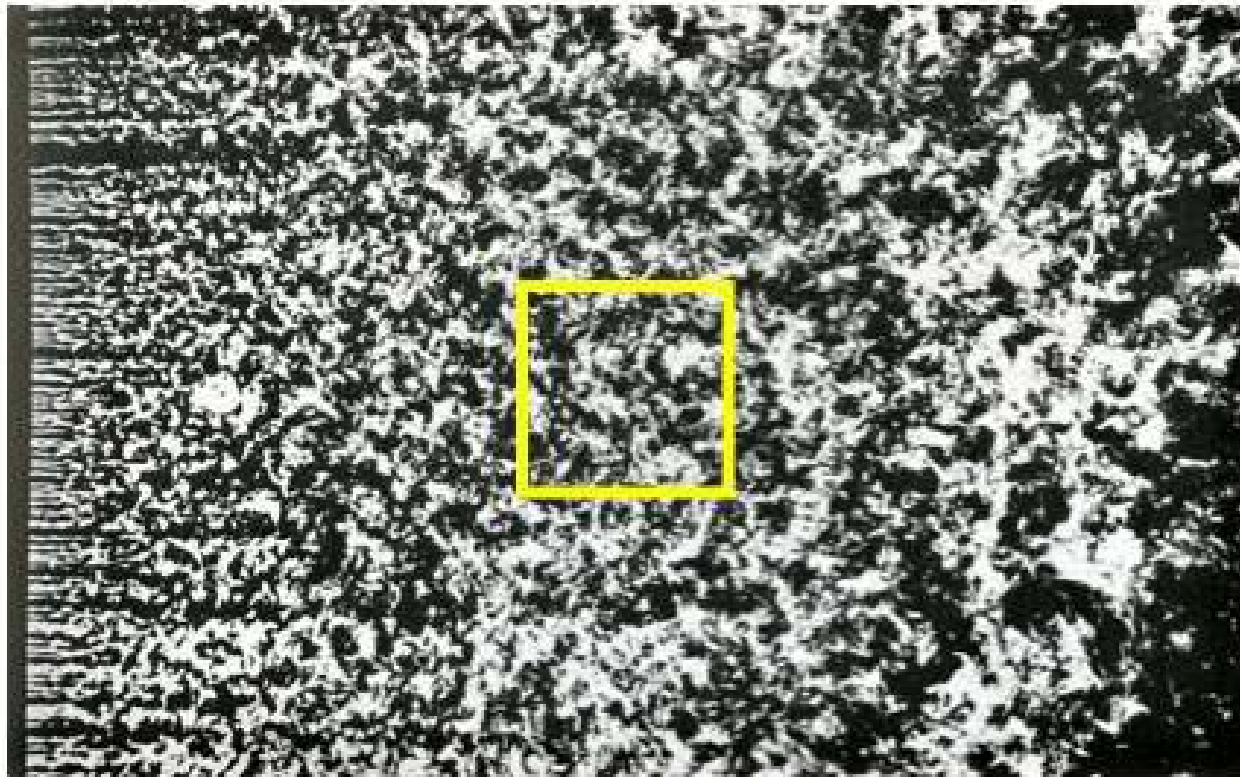
$$\tau_{ij}^{\hat{\quad}}, \tau_{ij}^{\bar{\quad}} \rightarrow \text{same } C$$

$$\rightarrow C = C(\bar{u}_i)$$

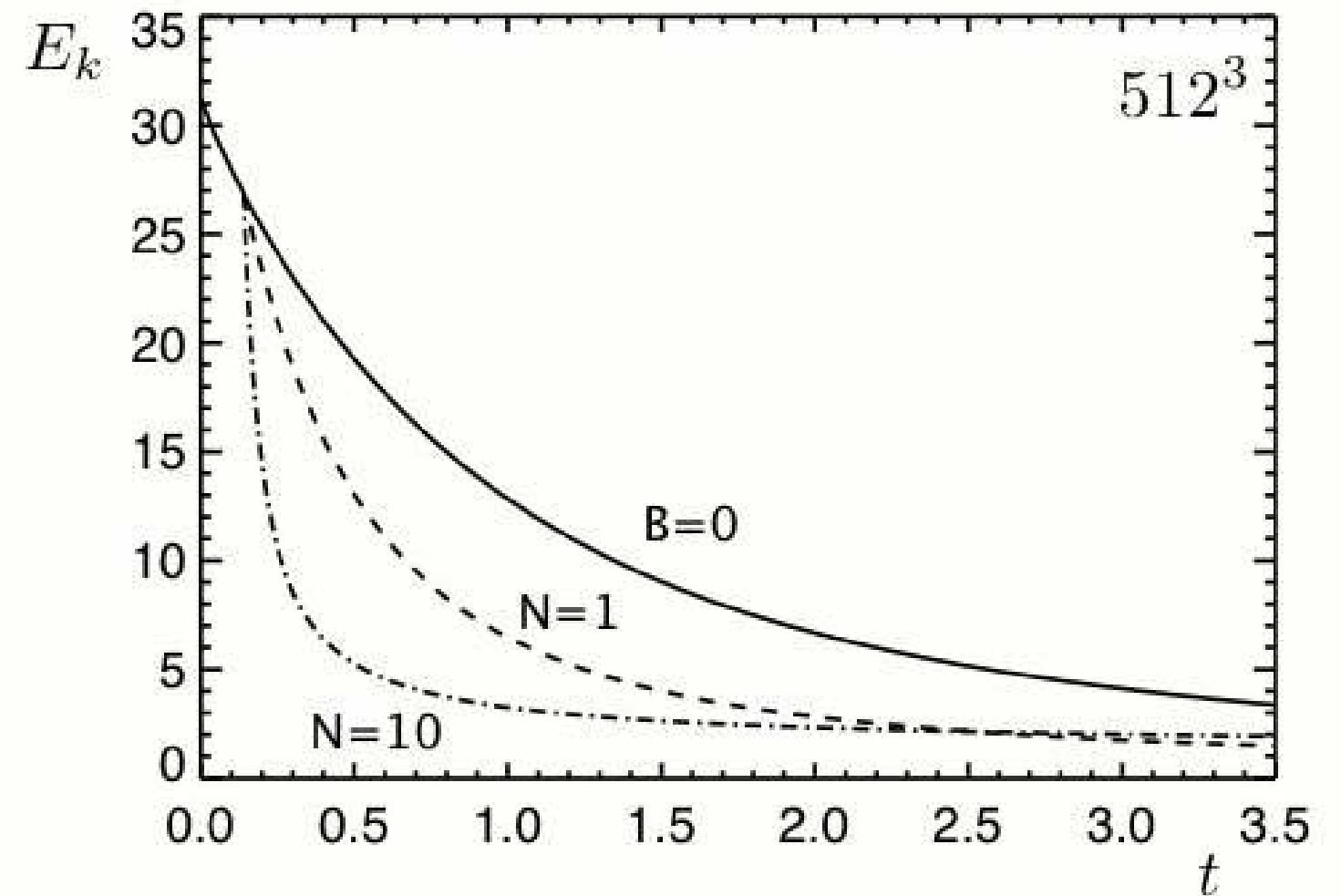
$$\tau_{ij} = -2C(\bar{u}_i)\Delta^2 \sqrt{2S_{ij}S_{ij}}S_{ij}$$

Dynamical Model

Decaying turbulence

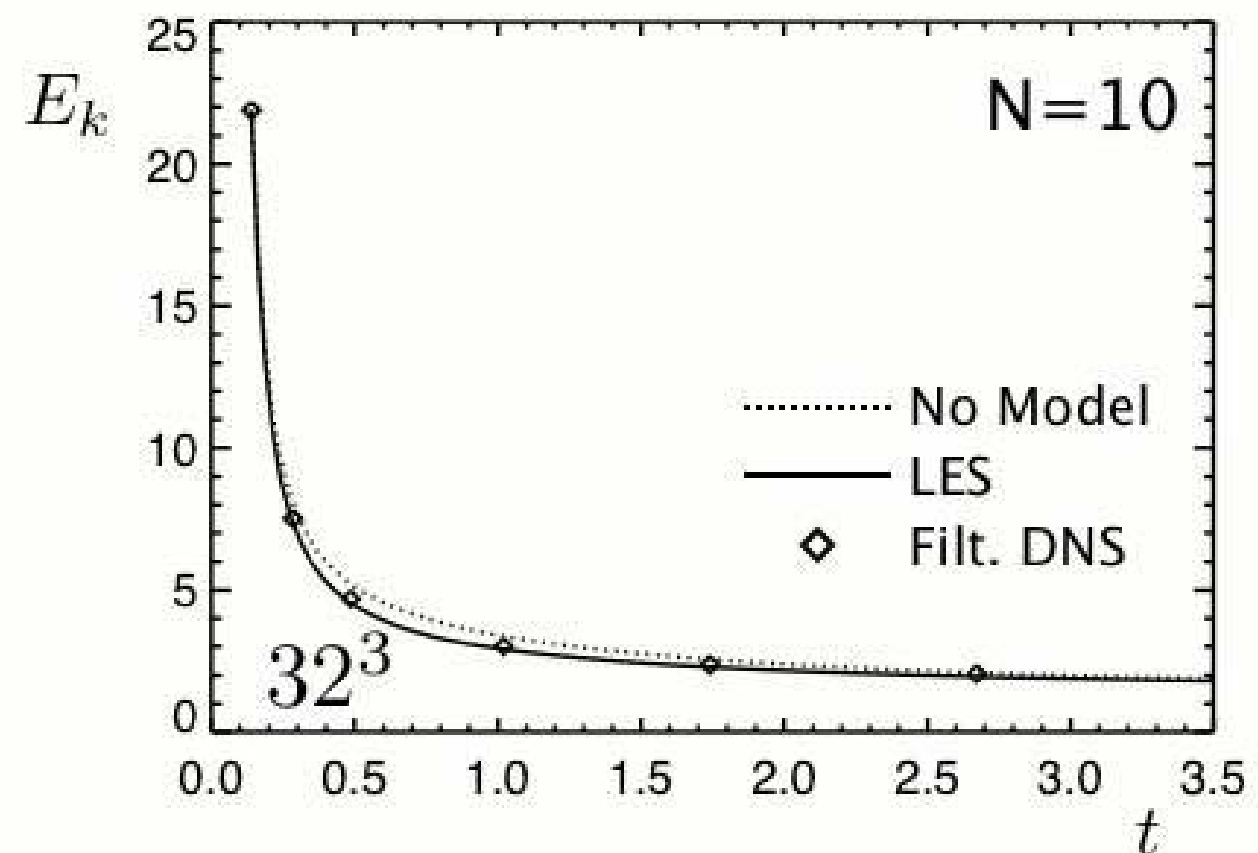
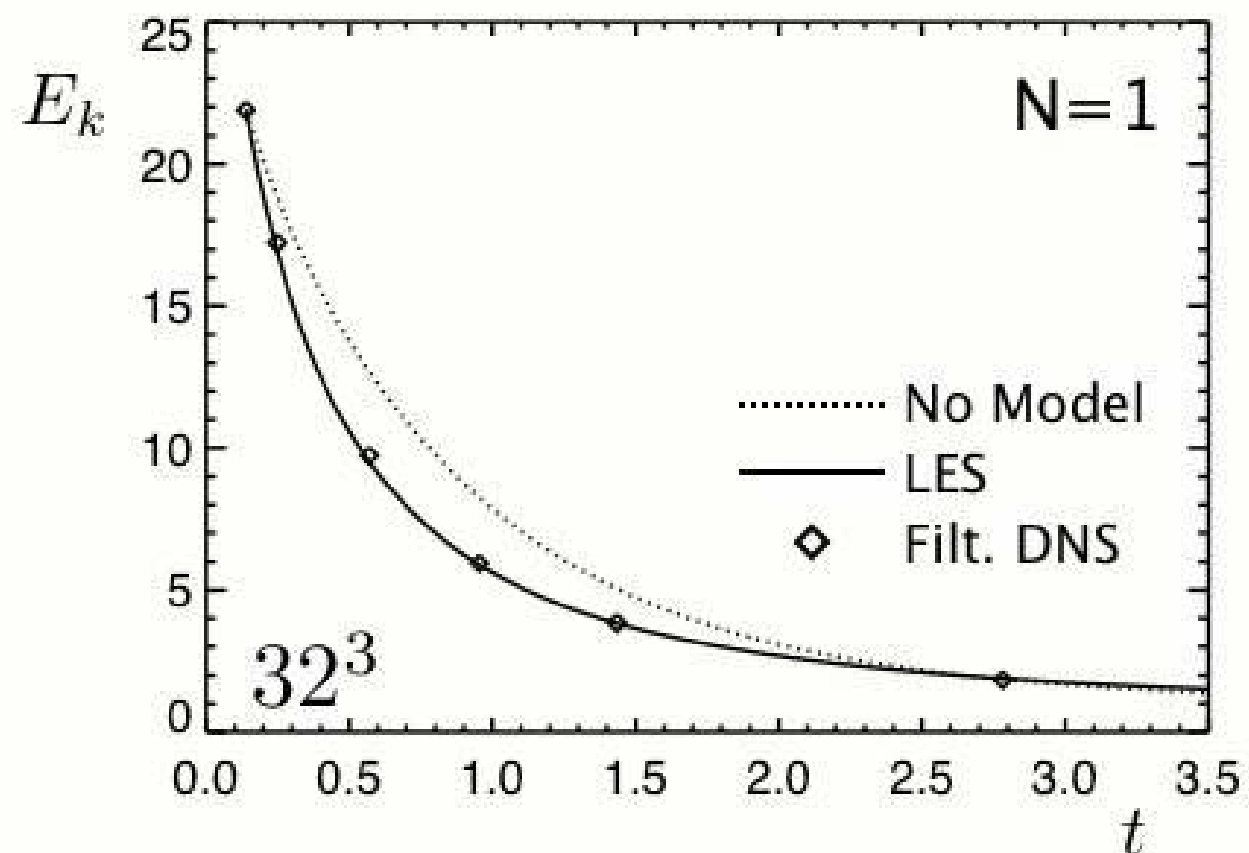
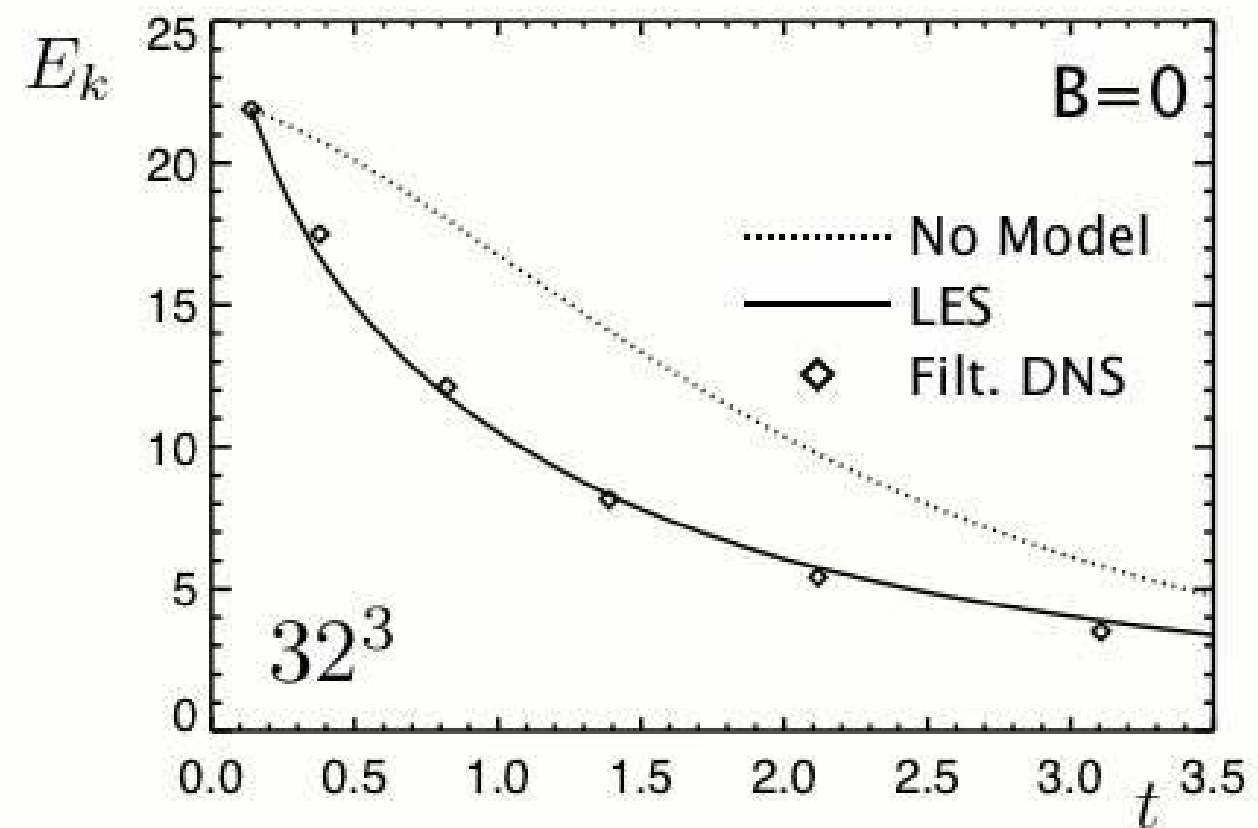
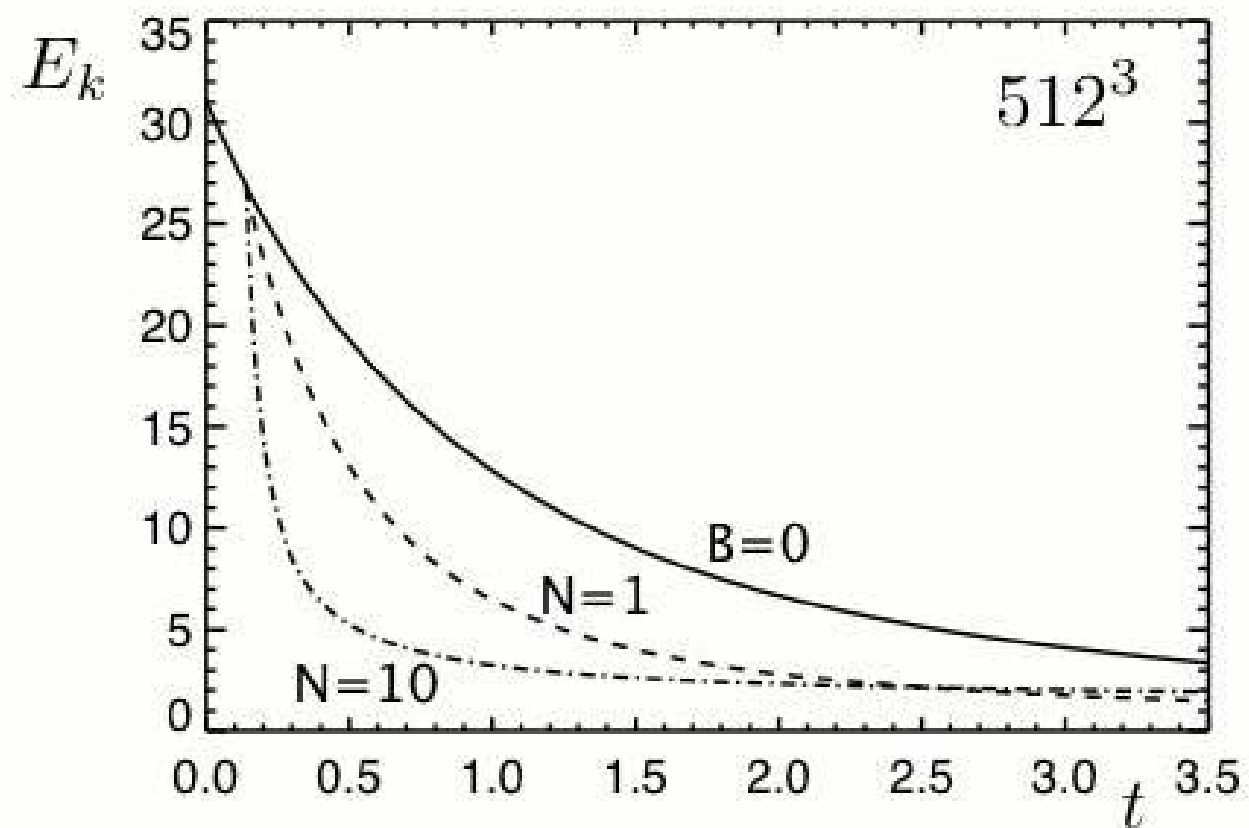


(Photo: Van Dyke M. An Album of Fluid Motion)

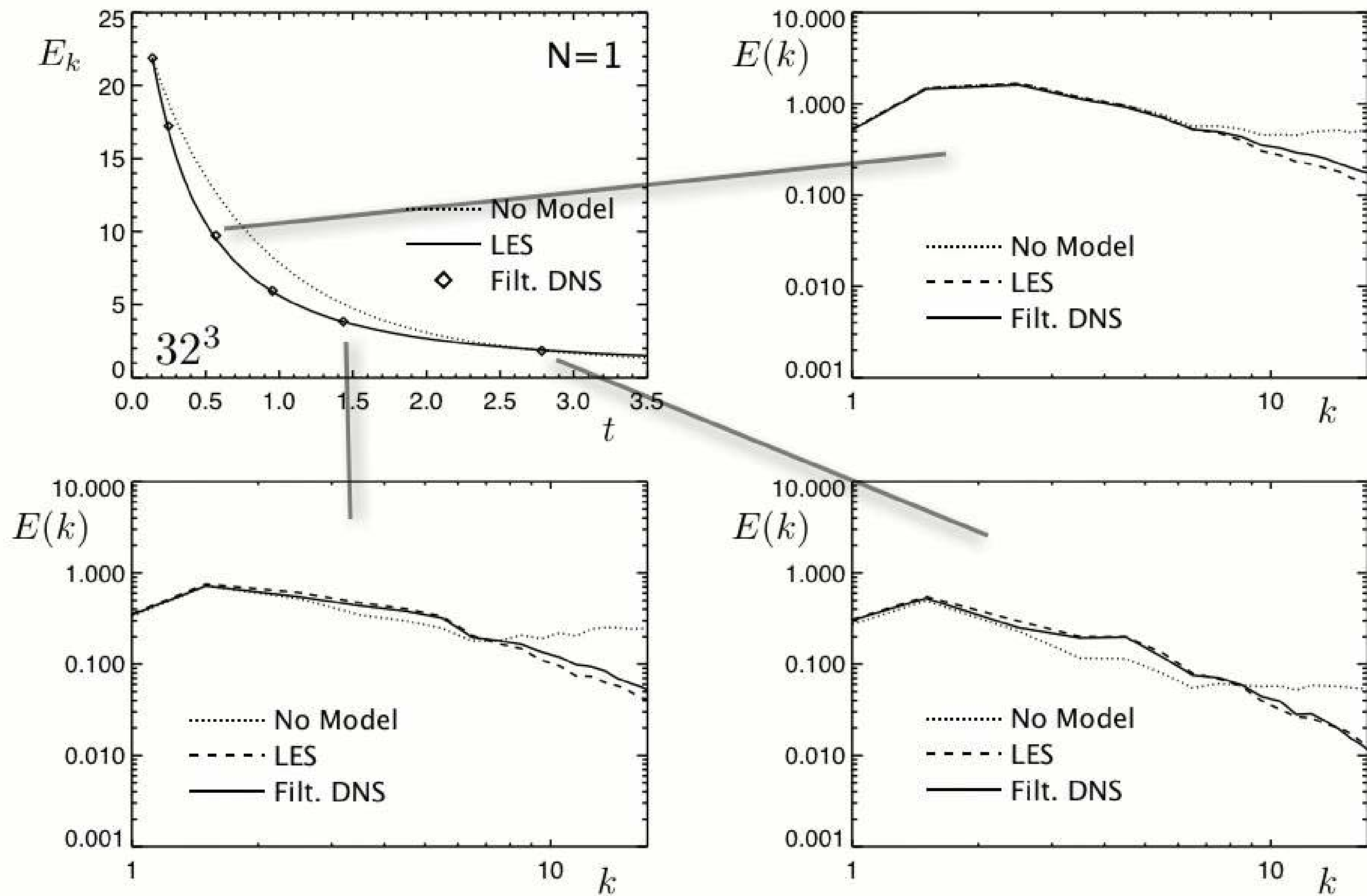


BK, Moin (2003)

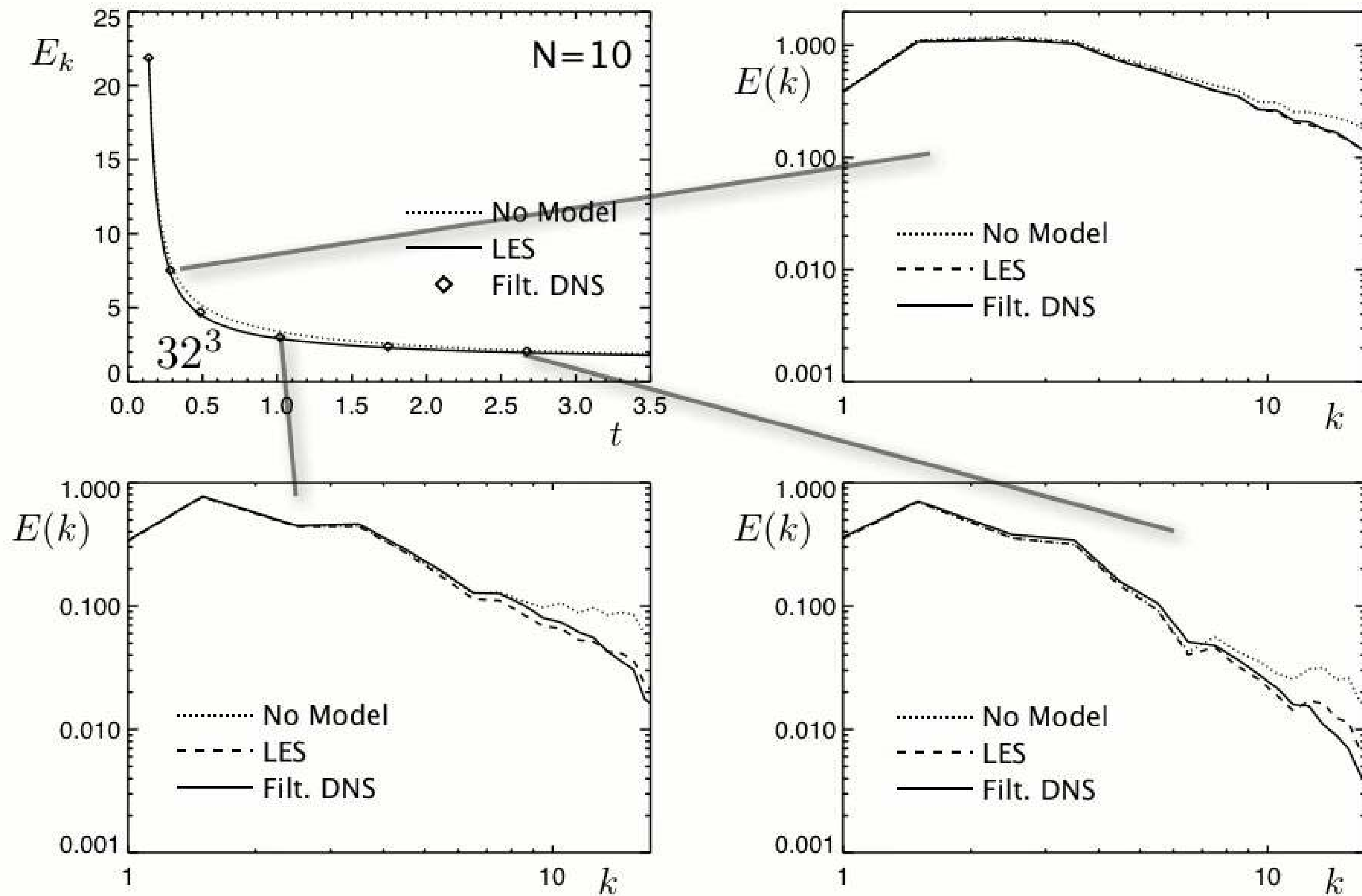
DNS versus LES



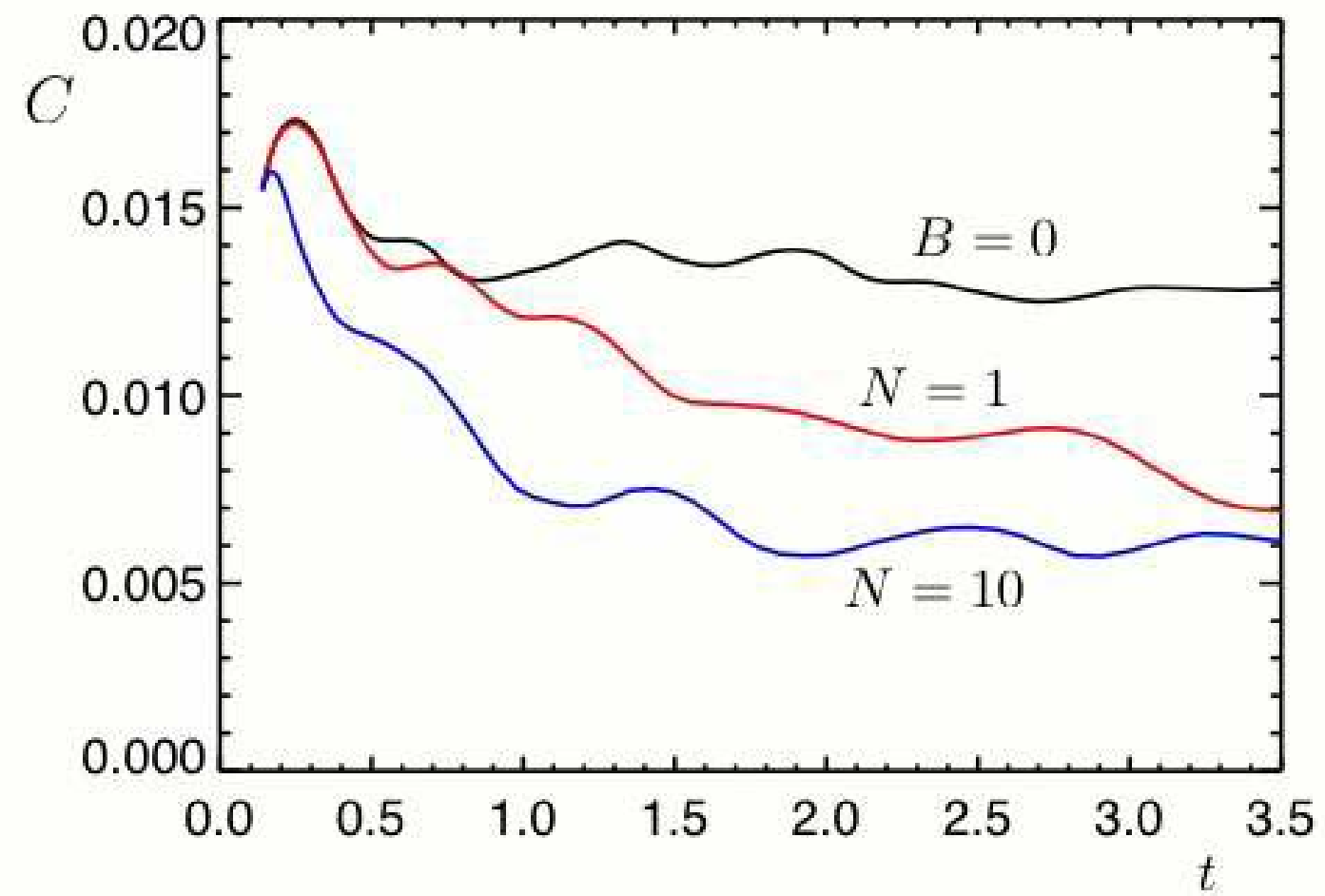
Energy Spectra N=1



Energy Spectra N=10

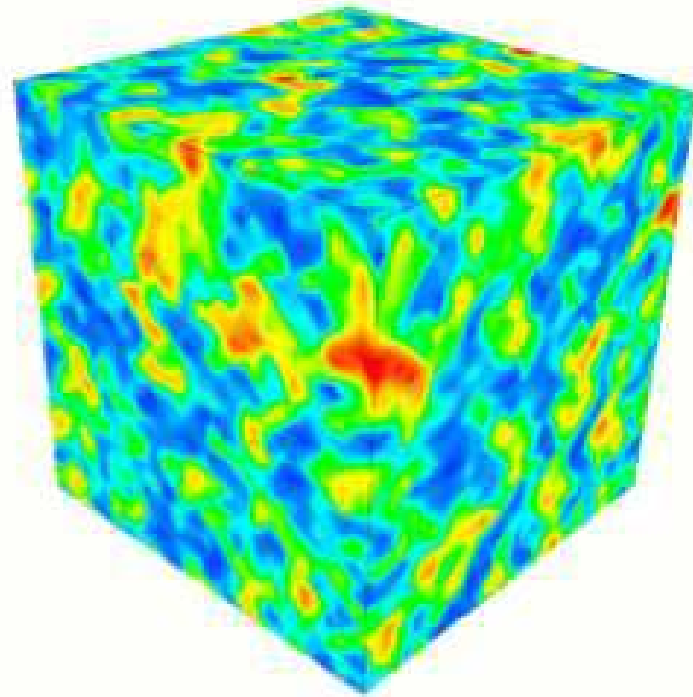


Dynamic constant

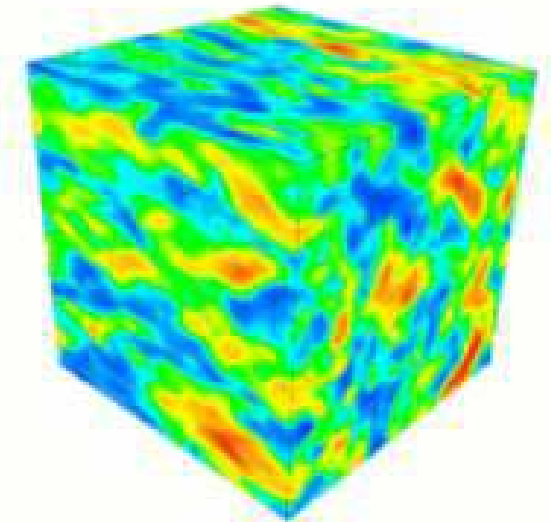
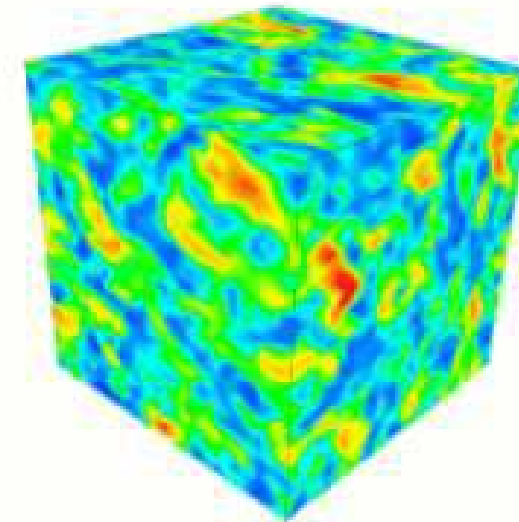
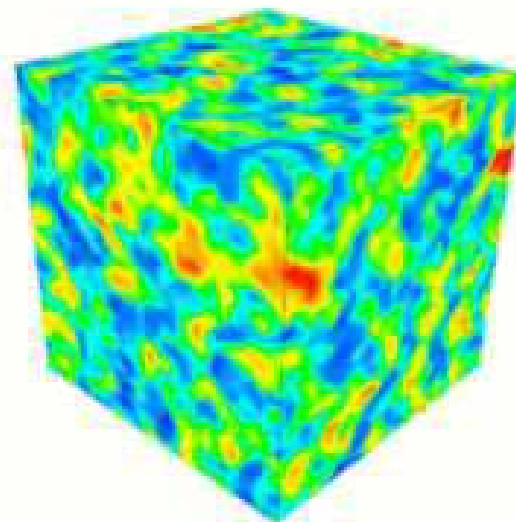
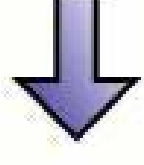
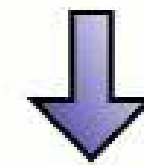
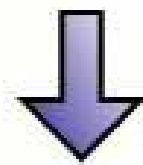
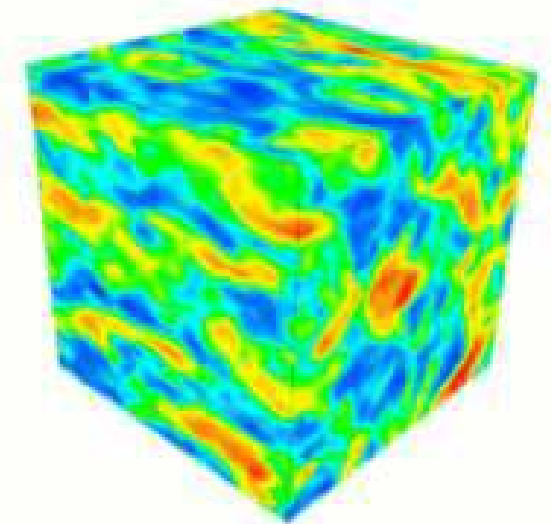
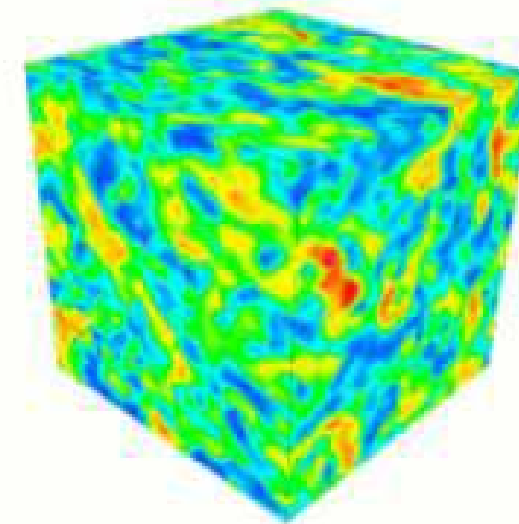
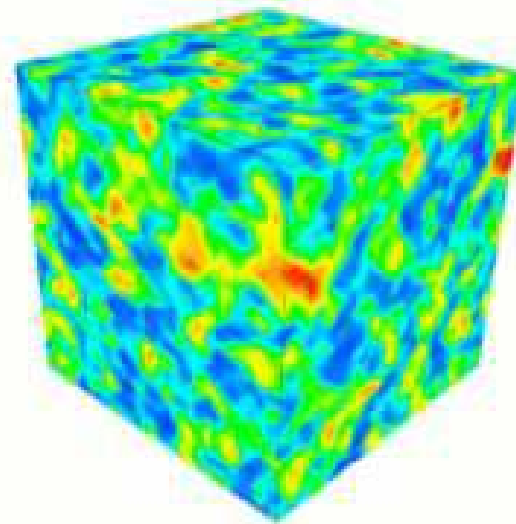


Energy contours N=1

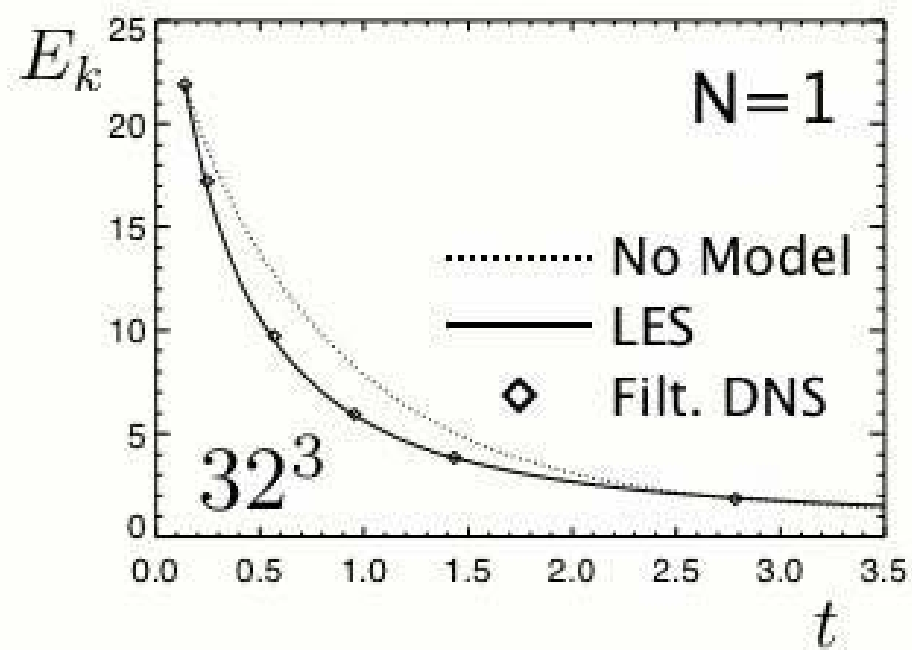
Initial flow



Filtered DNS 32^3

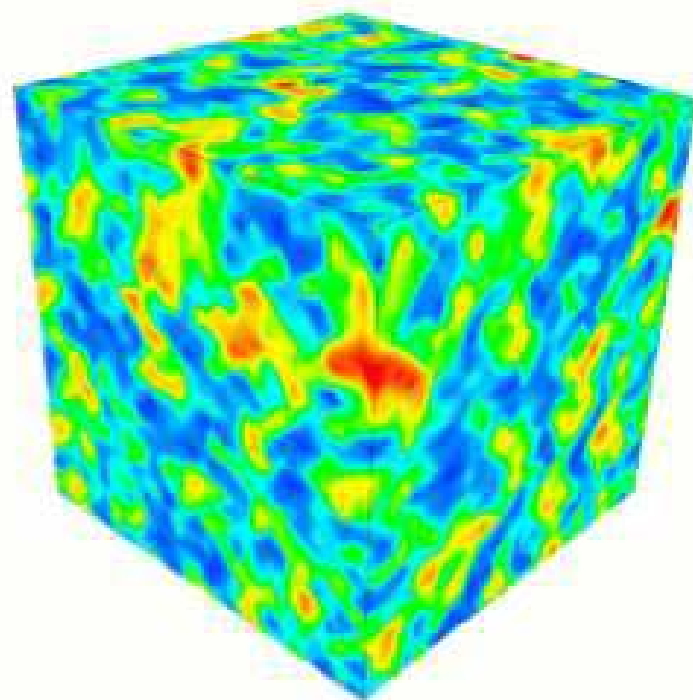


LES 32^3

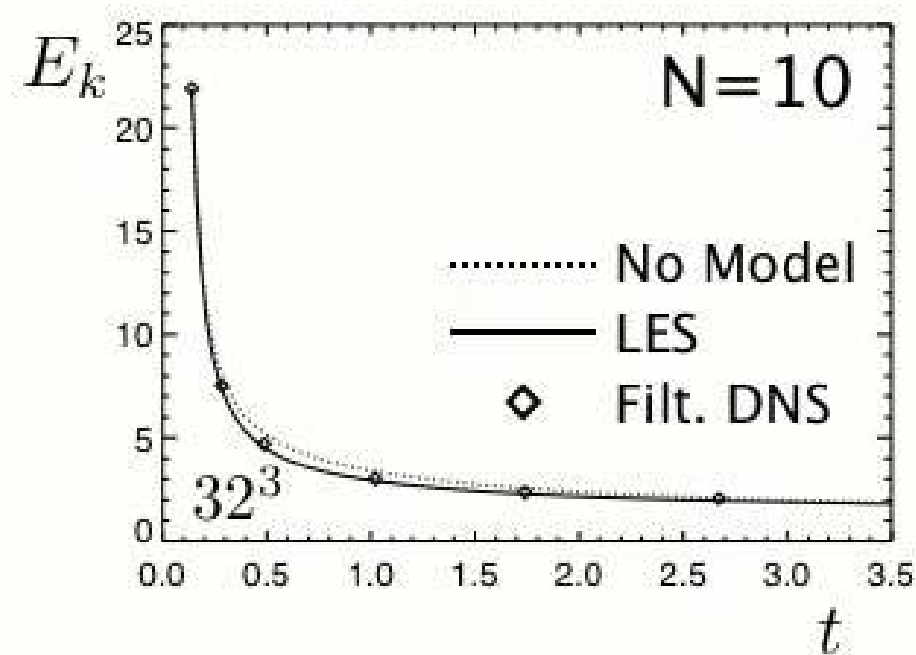
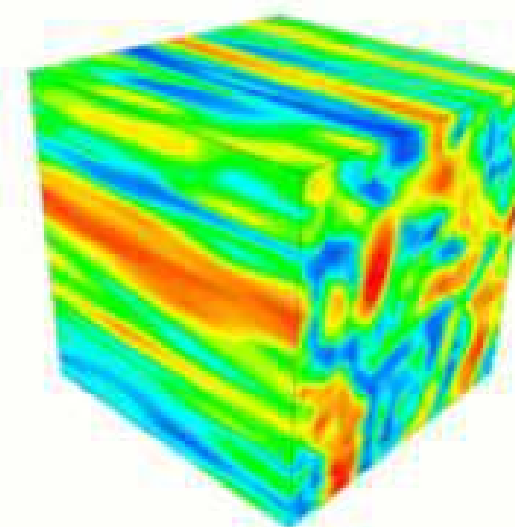
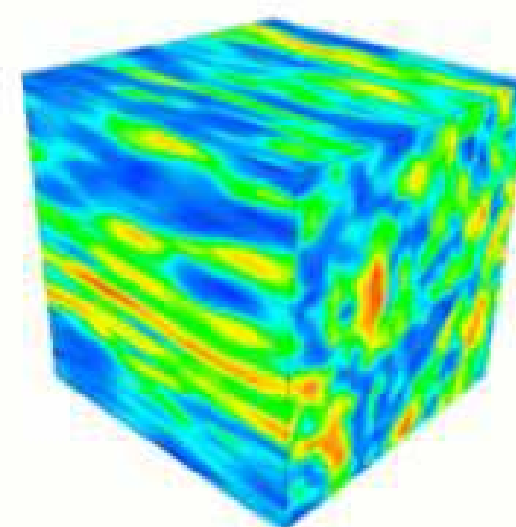
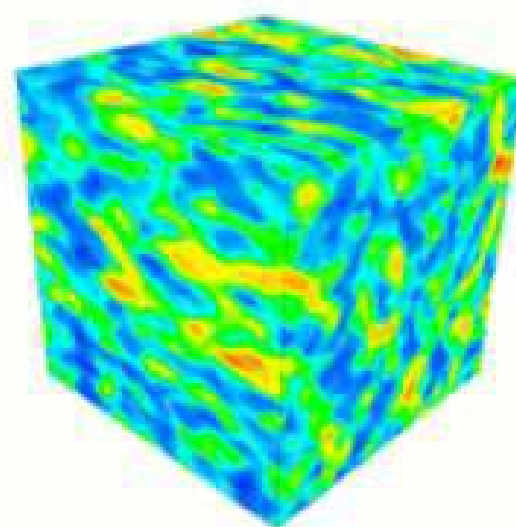
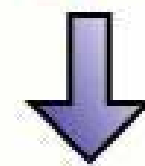
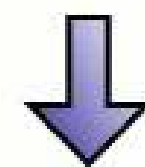
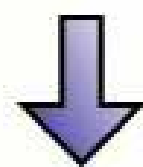
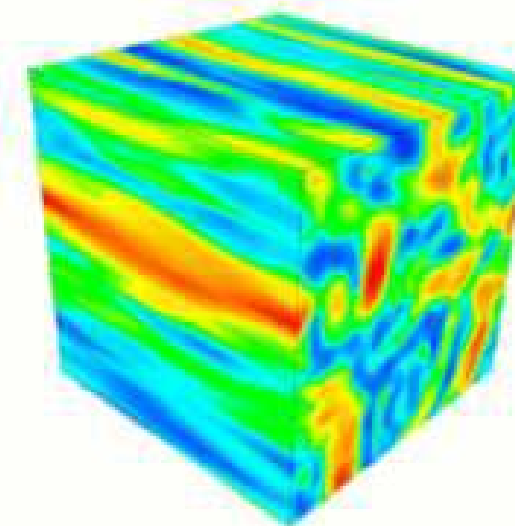
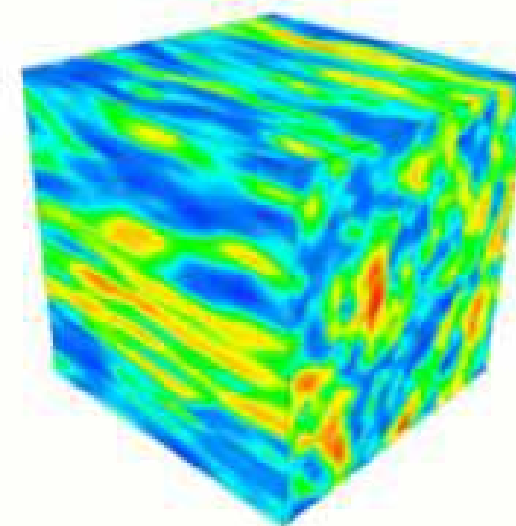
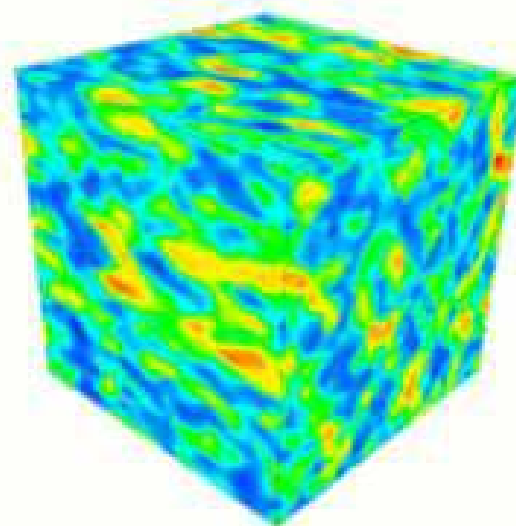


Energy Contours N=10

Initial flow



Filtered DNS 32^3



LES 32^3

Conclusions

- Turbulence is a complex process for which very few analytical results are known
- Numerical methods exist but they require theoretical model development in order to explore realistic flows
- Large-Eddy Simulations are a powerful tool for simulating flows at a lower computational cost
- Large-Eddy Simulations are widely used for engineering flows in complex geometries
- Only limited work has been devoted to this method in the case of MHD turbulence